East Midlands Gateway Phase 2 (EMG2)

Document DCO 6.13J/MCO 6.13J

ENVIRONMENTAL STATEMENT

Technical Appendices

Appendix 13J

Sustainable Drainage Statement – EMG2 Main Site

August 2025



The East Midlands Gateway Phase 2 and Highway Order 202X and The East Midlands Gateway Rail Freight and Highway (Amendment) Order 202X





ENVIRONMENT

SEGRO (Properties) Ltd East Midlands Gateway 2 Diseworth Sustainable Drainage Statement – EMG2 Works



ENVIRONMENT

SEGRO (Properties) Ltd
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Sustainable Drainage Statement – EMG2 Works

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August 2025



DOCUMENT ISSUE RECORD

Document Number:	EMG2-BWB-ZZ-XX-RP-CD-0001_SD\$ (EMG2 Works)
BWB Reference:	220500_SD\$ (EMG2 Works)

Revision	Date of Issue	Status	Author:	Checked:	Approved:
P01	20/05/2025	\$2	Matthew Bailey BSc (Hons)	Rowan Jobling BEng (Hons)	Chris Dodd BEng (Hons) IEng MICE
P02	13/06/2025	\$2	Matthew Bailey BSc (Hons)	Rowan Jobling BEng (Hons)	Chris Dodd BEng (Hons) IEng MICE
P03	25/06/2025	\$2	Matthew Bailey BSc (Hons)	Rowan Jobling BEng (Hons)	Chris Dodd BEng (Hons) IEng MICE
P04	25/07/2025	\$2	Matthew Bailey BSc (Hons)	Robin Green BSc (Hons)	Rowan Jobling BEng (Hons)
P05*	01/08/2025	\$2	Matthew Bailey BSc (Hons)	Robin Green BSc (Hons)	Rowan Jobling BEng (Hons)
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^{*}Update to appendices only

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1. INTRODUCTION

- 1.1 A Sustainable Drainage Statement (SDS) sets out the principles of drainage design for a development and summarises the reasoning behind the chosen design. This includes justification of specific flow rates, volumes of attenuated storage, as well as the appropriate level of treatment to be provided to surface water runoff.
- 1.2 This SDS has been produced by BWB Consulting on behalf of SEGRO (Properties) Ltd in respect of a Development Consent Order (DCO) for East Midlands Gateway 2 (EMG2), with this SDS report forming an appendix to the Environmental Statement (ES) submitted in support of the DCO.
- 1.3 A Flood Risk Assessment (FRA) has been developed for the site (reference: EMG2-BWB-ZZ-XX-T-W-0001_FRA) and this SDS accompanies the FRA.
- 1.4 The proposed development is to be submitted for a DCO, and as such the details have been developed in consultation with the relevant statutory bodies relating to flood risk and drainage for the site.
- 1.5 The Lead Local Flood Authority (LLFA) for the site are Leicestershire County Council (LCC). The LLFA are not the prescribed consultee under the DCO process; however North West Leicestershire District Council, the Local Planning Authority (LPA), are. As the LPA is not the LLFA for the site, the Environment Agency (EA) have been deferred to as the relevant body to comment on the surface water drainage strategy. Despite this, as the LLFA is the body responsible for surface water flood risk in relation to planning, LCC have been consulted through the DCO consultation stage and will comment of the surface water drainage proposals, via the EA.
- 1.6 Severn Trent Water (STW) are responsible for waste water disposal.

Situational Context & Associated Development

1.7 The proposed development comprises a number of interrelated component parts as follows, and collectively they are referred to as the EMG2 Project:

• EMG2 Works:

- o Construction of logistics and advanced manufacturing development and ancillary buildings (DCO, Works No. 1);
- o Construction of road infrastructure (DCO, Works No. 2);
- o Construction of bus interchange (DCO, Works No. 3);
- o Construction of HGV parking (DCO Works No. 4);
- o Provision of hard and soft landscaping (DCO Works No. 5);
- o Creation of a Community Park (DCO, Work No. 21); and
- o Upgrade of the EMG1 substation (DCO, Work No. 20)1.

¹ Note – As the existing substation is drained via the existing EMG1 drainage system, these specific works have been assessed within the EMG1 Works SDS report (reference: EMG2-BWB-ZZ-XX-RP-CD-0002_SDS (EMG1 Works))



Highways Works

- o A453 access junction works to the EMG2 Main Site (Works No. 6);
- o Hyam's Lane works (Works No. 7);
- o Works to the M1 northbound (Works No. 8);
- o Construction of link road from the M1 northbound to the A50 westbound (Works No. 9);
- o Works to the A50 westbound (Works No. 10);
- o Works to the link road from the M1 southbound and A50 eastbound to M1 Junction 24 (Works No. 11);
- o Works to the west side of the M1 Junction 24 roundabout and A453 northbound approach (Works No. 12a);
- o Works to the east side of the M1 Junction 24 roundabout and A453 southbound approach (Works No. 12b);
- o Improvements to the EMG1 access junction (Works No. 13);
- o Construction of the Active Travel Link between the EMG1 access junction and the A453 west of Finger Farm roundabout (Works No. 14);
- o Provision of an uncontrolled crossing of the A453 at the East Midland Airport signalised access junction (Works No. 15);
- o Works to M1 northbound signage on the approach to M1 Junction 23A (Works No. 16);
- o Works to Long Holden (Works No. 17);
- o Works to the A42/A453 Finger Farm roundabout (Works No. 18); and
- o Upgrade to public footpath L57 to a cycle track (Works No. 19).

EMG1 Works

- o Construction of a new rail-served warehouse building on land adjacent to the rail-freight terminal referred to as Plot 16 (MCO, Works No. 3A) together with associated access and drainage infrastructure, (MCO, Works No. 5A) and landscaping (MCO, Works No. 6A).
- o Alterations to the maximum permitted height of gantry cranes at the rail freight interchange by 4m, to 24m overall; An expansion of the EMG1 Management Suite by the EMG1 site entrance to cater for the additional demand on management facilities resulting from EMG1 (MCO, Works No. 3B);
- o Enhancements to the Public Transport Interchange by way of the installation of EV charging infrastructure for buses and provision of a drop-off layby adjacent to the transport hub (MCO, Works No. 5B and 5C); and
- o Provision of a signalised crossing over the EMG1 exit road approach to the access junction to EMG1 (MCO, Works No. 8A) connecting to the drop-off layby.
- 1.8 An illustrative site location plan is provided as **Figure 1.1**, which also identifies the approximate extent of the development component parts.



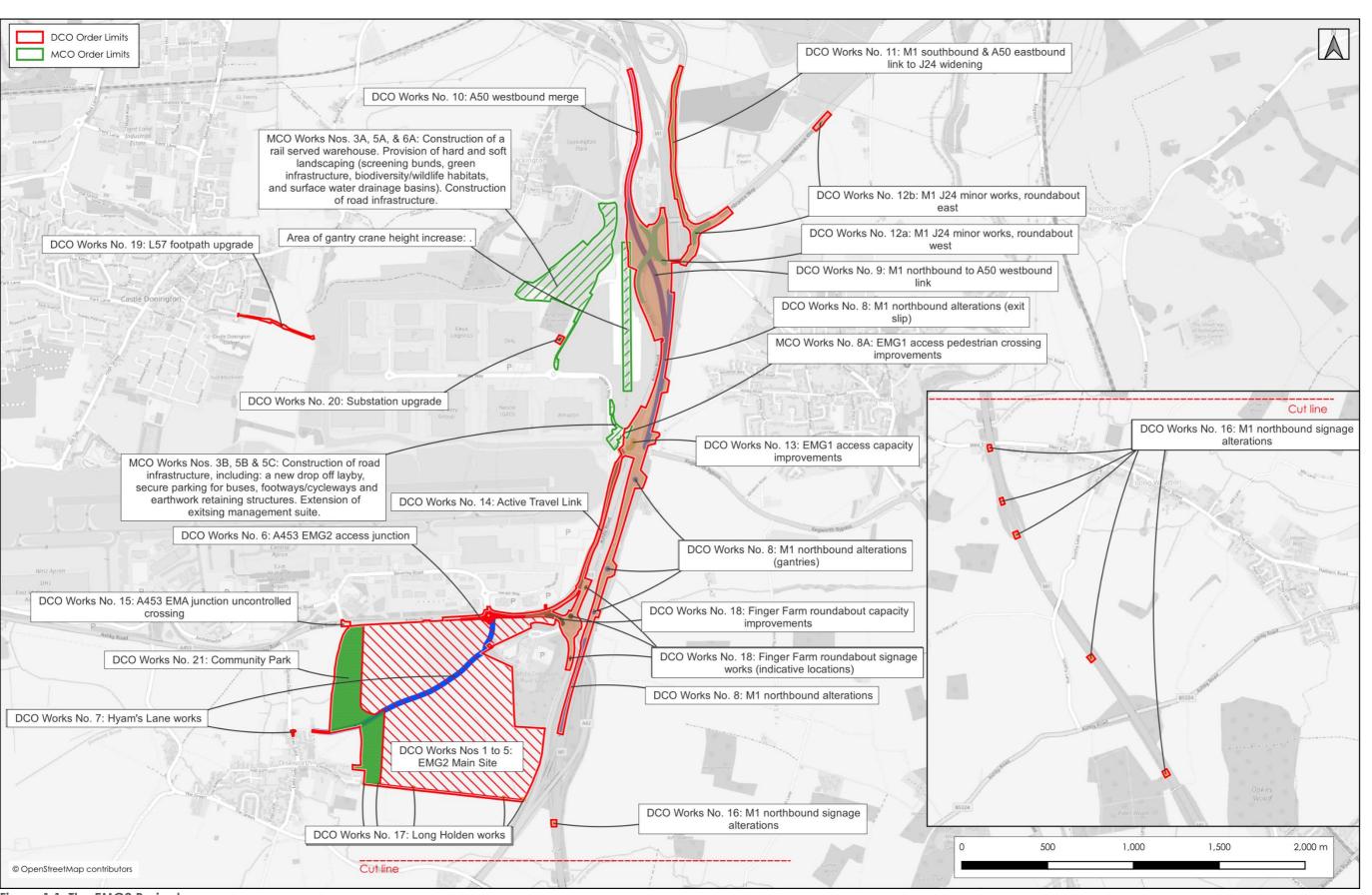


Figure 1.1: The EMG2 Project

- 1.9 This SDS has been prepared in relation to the 'EMG2 Main Site' and the adjacent area for the proposed Community Park (DCO Works No. 21), which are referred to as 'the site' throughout this report.
- 1.10 The EMG1 Works and Highway Works have been reviewed under separate cover (references: EMG2-BWB-ZZ-XX-RP-CD-0002_SD\$ (EMG1 Works) and EMG2-BWB-ZZ-XX-RP-CD-0003_SD\$ (Highways Works), respectively.
- 1.11 Refer to Document DCO 2.5 for the parameters plan. Contextual information for the site is provided within **Table 1.1**.

Table 1.1: Site Details

Table 1.1. Sile Details	
Site Name EMG2 Main Site & Community P	
NGR (approx.)	SK459250
Approximate Area (ha)	104 (approx.)
Proposed Contributing Area (ha)	69.08 (approx.)
Development Type	Class B8/B2 Office and Warehouse, community park
Lead Local Flood Authority	LCC
EA Area	East Midlands
Sewerage Undertaker	STW

Sustainable Drainage Guidance

Guidance Documents

- 1.12 This SDS and associated drainage strategy has been written with reference to the following guidance documents:
 - LCC's Interim LLFA Guidance Note: Planning and Development in Leicestershire2;
 - The DEFRA Non-Statutory Technical Standards for SuDS (2015)3;
 - The National Policy Statement for National Networks⁴ (NPSNN);
 - The Department for Transport (DfT) and National Highways (NH) Strategic road network and the delivery of sustainable development guidance (reference: DfT Circular 01/2022)⁵; and
 - The CIRIA C753 SuDS Manual⁶.

² Interim LLFA Guidance Note: Planning and Development in Leicestershire -Rev A (Leicestershire County Council, October 2018)

^{3 2015,} DEFRA. Non-statutory technical standards for sustainable drainage systems

⁴ National Policy Statement for National Networks, Department for Transport, March 2024

⁵ Strategic road network and the delivery of sustainable development guidance (Department for Transport and National Highways, December 2022)

⁶ The SuDS Manual Version 6 (CIRIA, 2019)

Climate Change and Urban Creep Allowances

1.13 The site is located within the Soar Management Catchment within the Humber River Basin District. Table 2 from the EA's 'Flood risk assessments: climate change allowances', included as **Table 1.2**, shows the anticipated changes in peak rainfall intensity for the site

Table 1.2: Soar Management Catchment Peak Rainfall Allowances

Soar Management Catchment Allowance	Total Potential Change Anticipated for the '2050s' (Lifetime up to 2060)	Total Potential Change Anticipated for the '2070s' (2061 to 2125)		
1 in 30-Year Rainfall Event				
Upper End	35%	35%		
Central	20%	25%		
1 in 100-Year Rainfall Event				
Upper End	40%	40%		
Central	20%	25%		

- 1.14 The proposed development is anticipated to have a lifespan of up to 75 years, therefore the 2070's epoch central allowance will be used to assess the impacts of climate change for the proposed surface water drainage strategy. Sensitivity testing has been undertaken using the 2070's epoch upper end allowance to ensure that there is no increase in flood risk elsewhere and the built development will be safe from surface water flooding over the anticipated lifetime of the proposed development.
- 1.15 Based on the above guidance, an allowance of 25% will be applied to the 1 in 100-year return period within the drainage design calculations, with sensitivity testing using a 40% allowance to the 1 in 100-year return period. During the detailed design stage a 25% climate change allowance, with a 35% sensitivity test, should be applied to the 1 in 30-year return period within the drainage design calculations. As the development is built out, the latest EA climate change allowance should be reviewed and used for the detailed design calculations for each phase of the development.
- 1.16 Based on the proposed development use, no urban creep allowance has been applied to the drainage design calculations.

2. EXISTING CONDITIONS

- 2.1 The site is bound to the north by East Midlands International Airport (EMIA) beyond Ashby Road (A453). Donnington Park Services is located adjacent to the north-east. The site is bound to the east by the A42 and the M1, the south by Long Holden public byway with agricultural fields beyond, and to the west by agricultural fields. The village of Diseworth is located approximately 150m south-west of the site. A public byway, known as Hyam's Lane, bisects the site from south west to north east.
- 2.2 The generalised topography of the site is shown in **Figure 2.1** with a full topographical survey (reference: 34529A_T_REV1) included as **Appendix 1**. The site is generally split into two topographical catchments located to the north and south of Hyam's Lane. The northern catchment falls generally in a westerly direction (towards the Hall Brook) with levels ranging from approximately 92.7metres Above Ordnance Datum (mAOD) in the northeast to approximately 67.1mAOD in the southwest. The southern catchment falls generally in a southerly direction with levels ranging from approximately 91.0mAOD in the northeast to approximately 52.6mAOD in the southeast.

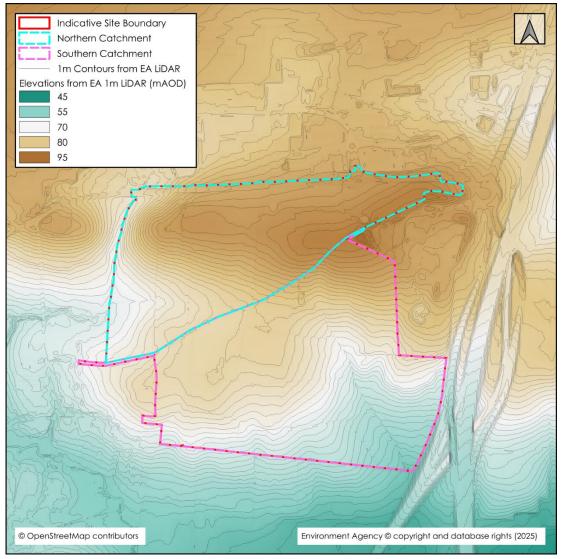


Figure 2.1: Existing Site Topography based on EA 1m LiDAR

- 2.3 The site is considered to be greenfield in nature and is currently utilised for agricultural practices. Hyam's Lane is made up of loose dirt and gravel.
- 2.4 The Hall Brook flows along a portion of the western boundary before flowing in a south-westerly direction to its confluence with the Diseworth Brook approximately 500m southeast of the site. A series of field ditches are present in the southeast corner of the site that drain via a piped connection (500mm diameter) which outfalls to larger pipe system (525mm to a 700mm diameter) which runs alongside the A42 and outfalls to the Diseworth Brook beneath the A42 road bridge.
- 2.5 STW sewer asset records (**Appendix 2**) show a public surface water sewer running parallel to the A42 culvert between the Donnington Services and the Diseworth Brook, outfalling just upstream of the A42 culvert. A public foul water rising main is shown to flow along Hyam's lane in a north-easterly direction. The rising main originates from a pumping station to the west off Grimes Lane and enters a public foul water gravity sewer to the north of the site beyond Ashby Road.
- 2.6 A Closed-Circuit Television (CCTV) survey (**Appendix 3**) shows the alignment of the existing piped system and surface water public sewer and confirm their ultimate outfall points into Diseworth Brook.
- 2.7 The site's location and local watercourse network are illustrated within **Figure 2.2**.

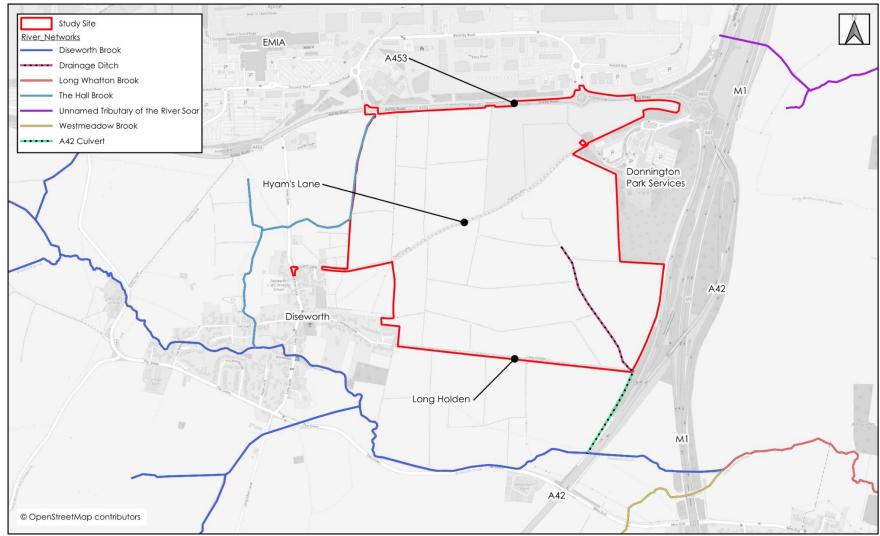


Figure 2.2: Site Location and Watercourse Network

2.8 British Geological Survey (BGS) mapping shows the site to be underlain predominantly by Gunthorpe Member – Mudstone, with thin bands of Gunthorpe Member – Siltstone, Dolomitic and Diseworth Sandstone. The bedrock geology is shown in **Figure 2.3**.

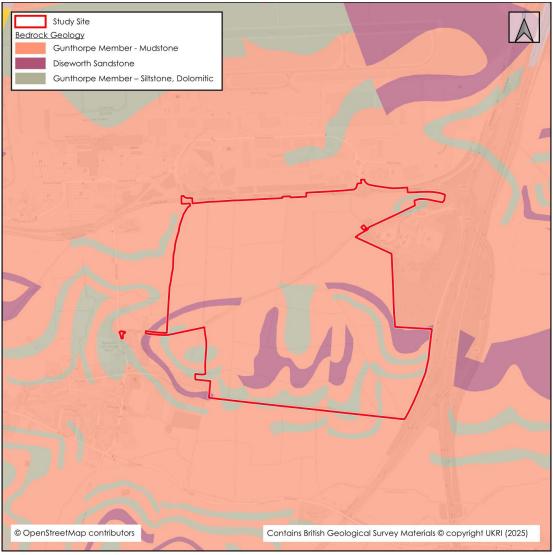


Figure 2.3: BGS Bedrock Map

2.9 Superficial deposits of Glaciofluvial Deposits, Mid Pleistocene – Sand and Gravel, Oadby Member – Diamicton and Head – Clay, Sand and Gravel are expected to be present within the site. The superficial deposits are shown in **Figure 2.4**.

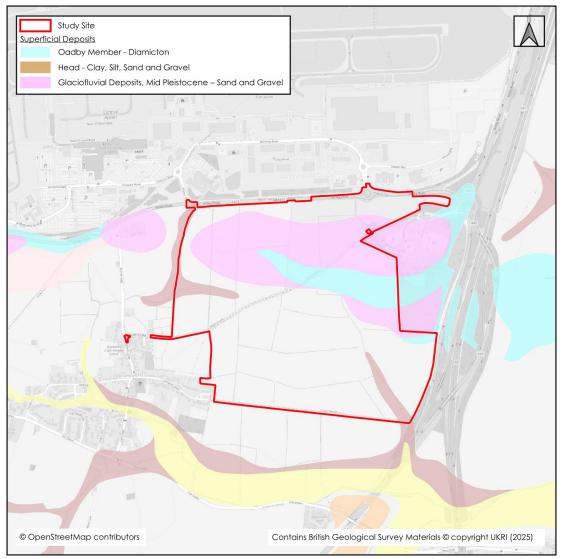


Figure 2.4: BGS Superficial Deposits

- 2.10 The Factual Ground Investigation Report (reference: 765514-01) prepared by Fairhurst outlines preliminary findings from intrusive ground investigations. This has confirmed the following ground conditions:
 - Topsoil (proven from the surface to a maximum depth of between 0.10 m and 0.85 m bgl);
 - Isolated occurrences of Made Ground (proven to a maximum depth of 0.20 m and 3.00 m bgl), with the deeper Made Ground encountered within the northern site area (location of anticipated historically infilled clay pits – TP08 and BH04);
 - Superficial deposits of The Oadby Member and Glaciofluvial Deposits (proven to maximum depths of 16.40 m bgl and 17.30 m bgl, respectively); and
 - Bedrock geology of The Gunthorpe Member and Diseworth Sandstone (proven to a maximum depth of 18.50 m bgl for the former, with the maximum depth of the latter not proven).

- 2.11 Groundwater monitoring suggested that two groundwater bodies are present between depths of 1.25m and 15.32m bgl (84.90m AOD and 52.7m AOD) within the Glaciofluvial, Weathered Gunthorpe Member and Gunthorpe Member. It was reported that the ground investigations found the ditch in the site to be dry throughout the works. Therefore, the watercourse is likely to be seasonally dry, with its main purpose to drain surface water runoff from the adjacent fields.
- 2.12 Based on the underlying geology across the site it is anticipated that there will be limited infiltration potential for surface water.
- 2.13 The accompanying FRA identifies that the site to be generally at low risk of flooding, although there are several potential surface water flow pathways that could form across the site. These potential flow paths are relatively shallow and generally originate from within the site itself. More details on the potential flood risk sources to the site and the proposed mitigation measures are outlined in the accompanying FRA.
- 2.14 It is understood that that the village of Diseworth to the southwest of the site is at risk of fluvial flooding associated with the Hall Brook and Diseworth Brook.
- 2.15 Based on the above information, the existing drainage regime at the site is for the northern catchment, as illustrated on **Figure 2.2**, to drain via surface runoff into the Hall Brook, before ultimately draining into Long Whatton Brook, via Diseworth Brook. The southern catchment drains via the existing A42 culvert, into Diseworth Brook and ultimately into Long Whatton Brook to the south east of the site.

Existing Runoff Rates

- 2.16 An assessment of the existing surface water runoff rates from the site has been undertaken on a litres per second per hectare basis. This is summarised within **Table 2.1**, with the associated calculations presented within **Appendix 4**.
- 2.17 The runoff rates have been estimated using the Flood Estimation Handbook (FEH) statistical method. This was undertaken using the UKSUDS Greenfield Runoff Rate Estimation Tool.

Table 2.1: Existing Runoff Rate per hectare from the Site

Return Period (Yrs.)	Runoff Rate (I/s/ha)
1	2.7
Mean Annual Flow Rate (QBAR)	3.3
30	6.6
100	8.4

Existing Runoff Volume

- 2.18 An assessment of the existing surface water runoff rates from the proposed contributing area used to inform the drainage design calculations has been made for a 1 in 100-year, 6 hour storm.
- 2.19 As the existing site is permeable, the runoff volume has been calculated using the predevelopment discharge calculator in Causeway Flow to be 21,232m³, results are included within **Appendix 5**.
- 2.20 Per hectare this equates to a greenfield runoff volume of 307m³.

3. SURFACE WATER DRAINAGE STRATEGY

- 3.1 A Concept Drainage Strategy is presented as Appendix 6, with the supporting attenuation calculations provided within Appendix 7.
- 3.2 The proposed contributing impermeable areas have been measured from the proposed parameters plan (Document DCO 2.5). The following impermeable area assumptions have been used:
 - Development plots and adjoining highways = 90%;
 - Embankments and bunds = 50%; and
 - Attenuating SuDS basins = 100%.
- 3.3 The assumed impermeable area for the proposed community park car park (100%) has been measured from the FPCR Illustrative Landscape Masterplan, which is enclosed on the Concept Drainage Strategy (Appendix 6) and is to be confirmed during the detailed design stage.
- 3.4 Based on the parameters plan, illustrative landscape masterplan and above impermeable area assumptions, the calculated contributing impermeable area is 69.08ha.
- 3.5 Given the nature of the DCO applications being approved based on the parameters plan, as the development is built out, the contributing areas may change and therefore the final attenuation requirements and discharge rates from the proposed development may differ from the calculations outlined within this SDS. The principles set out within this report should be carried through as the development is built out.

Drainage Hierarchy

- 3.6 The Planning Policy Guidance⁷ and the SuDS Manual⁸ identify that surface water runoff from a development should be disposed of as high up the following hierarchy as reasonably practicable:
 - i. into the ground (infiltration);
 - ii. to a surface water body;
 - iii. to a surface water sewer, highway drain, or another drainage system;
 - iv. to a combined sewer.
- 3.7 The aim of this is approach is to manage surface water runoff close to where it falls and mimic natural drainage as closely as possible.

⁷ Planning Practice Guidance. http://planningguidance.planningportal.gov.uk/. ⁸ The SuDS Manual (C753). CIRIA 2015.

<u>Infiltration</u>

3.8 Based on the existing ground conditions observed on site during the preliminary ground investigation, soakaway drainage is not considered to be viable for the proposed development.

Surface water body

- 3.9 As described within **Section 2**, the existing northern drainage catchment drains into the Hall Brook along the west site boundary, with the southern catchment draining into the existing A42 culvert, with the entire site ultimately draining into the Long Whatton Brook to the south east.
- 3.10 Given the existing fluvial flood risk to the village of Diseworth, it is proposed that the entire site will via the A42 culvert, located at the southeast corner of the site; thus, reducing the contribution of flows to the Hall Brook prior to its course through Diseworth.
- 3.11 Given that the entire site ultimately drains into Long Whatton Brook, cross-catchment transfer is not a significant concern with the proposed outfall strategy. However, In accordance with the NH DfT Circular 01/2022 paragraph 59, flows from the entire development will be limited to the existing catchment rates that currently drain to the A42 culvert (i.e., the southern catchment, as illustrated on **Figure 2.1**).
- 3.12 Paragraph 59 of the NH DfT Circular 01/2022 reads:

To ensure the integrity of the highway drainage systems, no new connections into those systems from third party development and proposed drainage schemes will be accepted. Where there is already an existing informal or formal* connection into the highway drainage system from a proposed development site, the right for a connection may be allowed to continue provided that the flow, rate and quality of the discharge into the highway drainage system remains unaltered or results in a betterment. The company may require a drainage management and maintenance agreement to be entered into to secure this requirement in perpetuity.

- * An informal connection refers to surface water run-off and a formal connection to an engineered connection.
- 3.13 Based on the above NH guidance, the proposed approach is considered to be acceptable.
- 3.14 Additionally, post-development hydraulic modelling has been undertaken as part of the FRA to assess the impacts of the drainage proposals to both Diseworth and downstream of the site. More information relating to the post-development hydraulic modelling is outlined within the accompanying FRA.

Peak Flow Control

- 3.15 In order to comply with the Non-Statutory Technical Standards for Sustainable Drainage Systems S2-S3°, runoff from greenfield developments should not exceed the equivalent greenfield rates for the 1 and 100-year return period events. Additionally, to comply with the NH DfT Circular 01/2022, the existing flow rates from the southern catchment into the A42 culvert should not increase post-development.
- 3.16 Therefore, to comply with the above peak flow control criterion, it is proposed to restrict the maximum discharge rate from the proposed development to the equivalent 1 in 1-year rate for the contributing areas measured within the southern catchment for all events up to the 1 in 100-year + 40% critical storm event. This is summarised within **Table** 3.2

Table 3.1: Existing Runoff Rates based on measured contributing areas

Catchment	Contributing Area (ha)	Return Period (Yr.)	Existing Runoff Rate (1/s)
		1	72.1
Northern	0.4.70	QBAR	88.2
Nomem	26.72	30	176.4
		100	224.4
	42.36	1	114.4
Southern		QBAR	139.8
souriem		30	279.7
		100	355.8
		1	186.5
Total	69.08	QBAR	228.0
Total		30	455.9
		100	580.3

^{9 2015,} DEFRA. Non-statutory technical standards for sustainable drainage systems

Table 3.2: Existing & Proposed Runoff Rates from the proposed development

Return Period (Yr.)	Existing Runoff Rate (1/s)	Proposed Discharge Rate (l/s)	Betterment (%)
1	186.5		39%
QBAR	228.0		50%
30	455.9	114.4	75%
100	580.3		80%
100 + 40%	-		-

- 3.17 This approach fulfils the necessary peak runoff control criteria and provides a significant betterment to the existing runoff rates leaving the site post-development, particularly during the higher return periods.
- 3.18 A review of the capacity of the A42 culvert has been undertaken to confirm that the proposed outfall has sufficient capacity to review flows from the proposed development. Based on the proposed maximum discharge rates outlined within Table 3.2, the A42 shas sufficient capacity to receive flows from the proposed development. The supporting technical note for this review is provided within Appendix 8.

Drainage Catchments

3.19 Given the scale of the proposed development, the proposed drainage system has been split into a total of nine cascading sub-catchments, all of which ultimately drain to the A42 culvert in the southeast site corner. The proposed sub-catchments are illustrated on the Conceptual Drainage Strategy (**Appendix 6**), with catchment details provided in **Table 3.3**.

Table 3.3: Existing & Proposed Runoff Rates from the proposed development

able 3.3. Existing & Proposed Kunoti Kales from the proposed development					
Catchment	Contributing Area (ha)	Maximum Discharge Rate (l/s)	Outfall Location		
1	23.12	89.0	Catchment 2		
2	2.73	42.8	Catchment 3		
3	20.18	33.4	Catchment 4		
4	0.82	77.6	Catchment 5		
5	0.48	78.4	Catchment 8		
6	4.64	7.7	Catchment 5		
7	15.35	25.4	Catchment 8		
8	0.78	105.0	Catchment 9		
9	0.99	114.4	A42 Culvert		
Total	69.08	114.4*			

^{*} Maximum discharge rate from final catchment to A42 culvert

Attenuated Storage

- 3.20 As the development proposals require a restricted runoff rate, it will be necessary to provide attenuated storage to balance the excess volume in a safe manner within the site.
- 3.21 The surface water storage should be located within the site in a position where it can receive runoff from the development and discharge from the site by gravity, and also in a position where it is hydraulically isolated from any fluvial floodplain or external surface water floodplain / overland flow route that may be present in the site.
- 3.22 Sufficient storage for events up to the 1 in 100-year storm with an allowance for climate change should be provided.
- 3.23 It is proposed that the majority of the attenuation for the proposed development will be provided within above ground attenuation basins located along the western and southern peripheries of the site. Where site constraints do not allow for enough space to utilise above ground attenuation, such as for Catchments 6 and 7, below ground cellular storage crates are proposed to provide the required attenuation volume on each respective plot.
- 3.24 Simulations have been run using Causeway Flow to identify the necessary storage provision for each catchment using FEH-22 rainfall data. The results are summarised in **Table 3.4** and calculations are included as **Appendix 7**.

Table 3.4: Attenuated Storage Requirements

Catchment	Critical Storm	Maximum Volume (m³) – 1 in 100-year + 25%	Critical Storm	Maximum Volume (m³) – 1 in 100-year + 40%*
1	720-min Winter	17,445	720-min Winter	19,675
2	7,200-min Winter	8,465	7,200-min Winter	9,475
3	1440-min Winter	16,655	1440-min Winter	18,815
4	720-min Winter	445	720-min Winter	550
5	1,440-min Winter	475	2,160-min Winter	525
6	1,440-min Winter	3,790	1,440-min Winter	4,280
7	960-min Winter	10,725	1,440-min Winter	12,100
8	960-min Winter	740	960-min Winter	850
9	720-min Winter	530	480-min Winter	585
Total	-	59,270	-	66,855

^{*} Sensitivity test to ensure that necessary storage is provided for upper end climate change allowance within basin design freeboard

- 3.25 At this conceptual stage it is expected that a minimum of 59,270m³ of attenuated storage will be required to cater for the maximum anticipated runoff volume for all storm durations up to the 1 in 100-year return period storm, including a 25% climate change allowance, extending to 66,855m³ during the 1 in 100-year + 40% climate change critical storm, which will be provided within the basin freeboard above the design water level.
- 3.26 It is envisaged that the final required attenuated storage volume will be determined as development is built out following the approval of the DCO.

Runoff Volume Control

- 3.27 The Non-Statutory Technical Standards for Sustainable Drainage Systems S4-S6¹⁰ states that where reasonably practical the runoff volume from a development for the 1 in 100-year 6 hour rainfall event should not exceed the runoff volume prior to development or redevelopment. Additionally, if practicable on previously developed sites, the runoff volume should not exceed the equivalent greenfield runoff volume. Where it is not reasonably practicable to constrain the volume of runoff from a development at or below the existing volume, then the runoff must be discharged in a manner that does not adversely affect flood risk, i.e.:
 - i. The additional runoff volume resulting from the development (the 'long term storage volume') should be discharged separately from the site at a rate of 2l/s/ha or less. Or,
 - ii. All the runoff volume from the development should be discharged at a rate equivalent to the mean annual flow rate (QBAR) rate under greenfield conditions or less. Or,
 - iii. All the runoff volume from the development should be discharged at a rate of 21/s/ha or less.
- 3.28 Due to the increase in impermeable surfacing within the site post-development, the 1 in 100-year 6-hour runoff volume will increase. However, as the drainage strategy proposes to limit the maximum discharge rate from the site below the existing greenfield QBAR rate for all events up to the 1 in 100-year + 40% critical storm, the volume criterion is met and long-term storage is not required.

Sustainable Drainage Systems

- 3.29 The drainage strategy proposes to utilise a series of detention basins and conveyance swales along the site periphery to provide both attenuation and water quality treatment to surface water flows prior to discharge from the site.
- 3.30 Given the nature of the DCO application, the internal plot layouts, and therefore the potential on-plot SuDS options, are not confirmed. As the plots are built out, the following SuDS should be incorporated into the on-plot drainage system prior to discharging into the spine drainage network conveying flows towards the periphery SuDS:
 - Filter Drains;
 - Permeable paving / bypass separator (for office parking areas); and
 - Full retention separators (for service yard areas).
- 3.31 The spine highway should utilise either roadside ditches / swales or silt traps and sump units for any highway gullys.

¹⁰ 2015, DEFRA. Non-statutory technical standards for sustainable drainage systems

- 3.32 It is proposed that a vortex separator (i.e., 'Downstream Defender' or similarly approved product) will be utilised downstream from the Catchment 9 vortex flow control to provide a final stage of surface water treatment as surface water is discharged from the site.
- 3.33 The detention basins and swales around the site periphery will be lined with an impermeable membrane to mitigate the risk of any potential pollutants infiltrating into the ground and contaminating the groundwater recharge in the vicinity of the site.
- 3.34 The detention basins will have a low flow channel and the incorporation of any ecological features will be confirmed at detailed design.
- 3.35 Based on the site's proximity to EMIA, the detention basins will be formed with a ridged base in a 'crinkle-cut' style to promote faster drain down times and discourage birds gathering during the lower return periods.

Water Quality

- 3.36 In accordance with the SuDS Manual a simple index approach to water quality risk management should be undertaken for the proposed development. This will be compiled to provide a comprehensive account of the water quality treatment provided by the proposed surface water drainage system.
- 3.37 The SuDS Manual Mitigation Index will be used to assess the treatment levels proposed in relation to the pollution hazard posed from the proposed land use(s). This methodology is adopted to ensure that surface water flows receive adequate treatment through all areas of the site prior to final outfall.
- 3.38 **Table 3.5** shows the pollution hazard indices for the land use classification(s) that are relevant to the proposed development, as described within table 26.2 in the SuDS Manual.

Table 3.5: Pollution Hazard Indices for Different Land Use Classifications

Land Use	Pollution Hazard Level	Total Suspended Solids (TSS)	Metals	Hydrocarbons
Industrial roofs	Low	0.3	0.2	0.05
Non-residential parking	Medium	0.7	0.6	0.7
Industrial sites	High	0.8	0.8	0.9

3.39 The SuDS Mitigation Indices that are relevant to the proposed development, at this stage, as described within table 26.3 of the SuDS Manual, are outlined in **Table 3.6.**

Table 3.6: SuDS Mitigation Indices

Type of SuDS	Mitigation Indices			
Component	TSS	Metals	Hydrocarbons	
Swale	0.5	0.6	0.6	
Permeable Pavement	0.7	0.6	0.7	
Detention Basin	0.5	0.5	0.6	
Bypass Separator*	0.8	0.6	0.9	
Full Retention Separator*	0.8	0.6	0.9	
Vortex Separator^	0.5	0.4	0.5	

^{*} Based on SPEL Enhanced Silt Retention bypass / full flow ¹¹ range (other products may vary) ^ Based on Hydro International Downstream Defender 'Advanced Vortex' ¹² (other products may vary)

- 3.40 The sitewide SuDS treatment system (i.e., series of detention basins and swales located along the west and south periphery of the site) will provide the majority of the water quality mitigation for the proposed development. Given the proposed development use, appropriate SuDS / proprietary treatment systems, in the form of bypass or full retention separators, will be used on each plot as required to provide a first stage of treatment prior to connecting into the site wide drainage system.
- 3.41 At this stage, it is anticipated that in addition to the site wide SuDS treatment system, the following on plot SuDS treatment measures will be incorporated, as a minimum:
 - Full retention separators for service yards; and
 - Bypass separators or permeable block paving for car parking areas;
- 3.42 The following SuDS treatment measures for each catchment land use is outlined within **Table 3.7** Please note that Catchments 2, 5, 8 and 9 have been excluded from **Table 3.7**, as these catchments only include earthwork batters, which are considered to have no pollution hazard risk. These catchments also drain via the sitewide SuDS treatment system and will therefore receive treatment from a minimum of one detention basin and the vortex separator, with additional treated to the catchments located further upstream within the sitewide drainage system.

11 SPEL Stormceptor Enhanced Silt Retention bypass (https://spelproducts.co.uk/spel-esr-bypass/) / full flow (https://spelproducts.co.uk/spel-esr-full-flow/) treatment system

12 Hydro International Downstream Defender 'Advanced Vortex' (https://hydro-int.com/en/products/downstream-defender?gl=1*hp5mv1* up*MQ..* gs*MQ..&gbraid=0AAAAADz81nmuhOElzqh5sqrGrEqmZFmaI)

Table 3.7: SuDS treatment measures for each catchment

Catchment	Land use	SuDS Treatment Measures		
1	Commercial Roof	Detention basin (8no.) + Swale (2no.) + Vortex Separator		
	Non-residential Parking	Bypass Separator / Permeable Paving + Detention basin (8no.) + Swale (2no.) + Vortex Separator		
	Service Yards	Full Retention Separator + Detention basin (8no.) + Swale (2no.) + Vortex Separator		
	Highways	Detention basin (8no.) + Swale (2no.) + Vortex Separator		
	Commercial Roof	Detention basin (7no.) + Swale (2no.) + Vortex Separator		
	Non-residential Parking	Bypass Separator / Permeable Paving + Detention basin (7no.) + Swale (2no.) + Vortex Separator		
3	Service Yards	Full Retention Separator + Detention basin (7no.) + Swale (2no.) + Vortex Separator		
	Highways	Detention basin (7no.) + Swale (2no.) + Vortex Separator		
4	Non-residential Parking	Detention basin (4no.) + Swale (2no.) + Vortex Separator		
	Commercial Roof	Detention basin (3no.) + Swale (2no.) + Vortex Separator		
,	Non-residential Parking	Bypass Separator / Permeable Paving + Detention basin (3no.) + Swale (2no.) + Vortex Separator		
6	Service Yards	Full Retention Separator + Detention basin (3no.) + Swale (2no.) + Vortex Separator		
	Highways	Detention basin (3no.) + Swale (2no.) + Vortex Separator		
7	Commercial Roof	Detention basin (2no.) + Swale (2no.) + Vortex Separator		
	Non-residential Parking	Bypass Separator / Permeable Paving + Detention basin (2no.) + Swale (2no.) + Vortex Separator		
	Service Yards	Full Retention Separator + Detention basin (2no.) + Swale (2no.) + Vortex Separator		
	Highways	Detention basin (2no.) + Swale (2no.) + Vortex Separator		

3.43 The pollution hazard rating and proposed SuDS Mitigation Index for each drainage Catchment is compared within **Table 3.8**. Where more than one SuDS component is proposed, a factor of 0.5 has been applied to the downstream (i.e., secondary and/or tertiary) treatment stages to account for the reduced performance due to reduced inflow concentrations.

Table 3.8: Comparison of Pollution Hazard Rating against Proposed Mitigation Index

	Land use	Pollution Hazard Rating		Proposed Mitigation Index			Sufficient Treatment Provided?	
Catchment		TSS	Metals	Hydrocarbons	TSS	Metals	Hydrocarbons	sonicieni neannem riovidea?
1	Commercial Roof	0.3	0.2	0.05	3.00	3.05	3.55	✓
	Non-residential Parking	0.7	0.6	0.7	3.45	3.40	3.95	✓
	Service Yards	0.8	0.8	0.9	3.55	3.40	4.15	✓
	Highways	0.8	0.8	0.9	3.55	3.40	4.15	✓
	Commercial Roof	0.3	0.2	0.05	2.75	2.80	3.25	✓
3	Non-residential Parking	0.7	0.6	0.7	3.20	3.15	3.65	✓
	Service Yards	0.8	0.8	0.9	3.30	3.15	3.85	✓
	Highways	0.8	0.8	0.9	3.30	3.15	3.85	✓
4	Non-residential Parking	0.7	0.6	0.7	2.00	2.05	2.35	✓
	Commercial Roof	0.3	0.2	0.05	1.75	1.80	2.30	✓
	Non-residential Parking	0.7	0.6	0.7	2.20	2.15	2.70	√
6	Service Yards	0.8	0.8	0.9	2.30	2.15	2.90	√
	Highways	0.8	0.8	0.9	2.30	2.15	2.90	√
7	Commercial Roof	0.3	0.2	0.05	1.50	1.55	2.05	√
	Non-residential Parking	0.7	0.6	0.7	1.95	1.90	2.45	✓
	Service Yards	0.8	0.8	0.9	2.05	1.90	2.65	✓
	Highways	0.8	0.8	0.9	2.05	1.90	2.65	✓

- 3.44 **Table 3.8** demonstrates that the proposed drainage system will provide significant treatment to surface water prior to discharge from the proposed development. It should be noted that for the on-plot non-residential parking water quality assessment, to provide a robust assessment, it is assumed that permeable paving will be used as this SuDS treatment measure provides a lesser pollution mitigation index score compared to bypass separators.
- 3.45 A Construction Environmental Management Plan (CEMP) will be prepared to support the DCO application and to ensure that the surrounding watercourses are not adversely affected during the construction stages.

Residual Risk and Designing for Exceedance

- 3.46 It is recommended that the final layout uses the proposed road infrastructure to provide drainage exceedance (overland flood flow) routes through the development and towards the periphery SuDS for events in excess of the capacity of the drainage system.
- 3.47 The detention basins have been designed to not flood during the 1 in 100-year + 40% critical storms, with additional freeboard provided above the sensitivity test events. In the event that the outfall for a basin becomes blocked, each detention basin flow control chamber will have a weir wall set above the anticipated 1 in 100-year +40% climate change critical storm water level, to provide a controlled location for water to overtop and drain into the downstream network, to be attenuated in the next detention basin, rather than immediately exceeding onto surrounding land.
- 3.48 If the Catchment 9 basin becomes blocked, exceedance flows will overtop and drain into the A42 culvert, as per the current conditions at the site.
- 3.49 The plots located within Catchments 6 and 7 should be designed such that any exceedance flows in the event of system blockage is kept on-plot and pools within the car parking and/or service yard areas.
- 3.50 In addition to the volume of storage provided within the main attenuation, there will be capacity within upstream pipes and manholes which has not been accounted for at this stage and a further level of redundancy to the network will therefore be provided.

4. MAINTENANCE

- 4.1 A management company will be appointed to maintain the SuDS features, including vegetation maintenance, trash screen clearing and regular outfall inspections. The inlet to the A42 culvert within the site boundary will also be included within the inspection and maintenance regime for the site.
- 4.2 Requirements for ongoing maintenance of the drainage network should form part of the Operation and Maintenance manual for the site and should be undertaken by the site management. Any specialist or proprietary products that are specified at detailed design should have a manufacturer specific maintenance regime which should be included within the document.
- 4.3 It is envisaged that the Operation and Maintenance manual will be developed at the detailed design stage, but some examples for the proposed detention basin, swales, and inlet to the A42 are provided below in **Table 4.1**, **Table 4.2** and **Table 4.3**, respectively.

Table 4.1: The SuDS Manual Typical Maintenance Schedule for Swales

Table 4.1: The SuDS Manual Typical I		Maintenance Schedule for Swales
Maintenance Schedule	Typical Frequency	Required Action
Regular Maintenance	Monthly	 Inspect inlets, outlets and overflows for blockages, and clear if required.
	Monthly (or as required)	 Remove litter and debris; and Inspect infiltration surfaces for ponding, compaction, silt accumulation, record areas where water is ponding for > 48 hours.
	Monthly (during growing season), or as required	Cut grass – to retain grass height within specified design range.
	Monthly for first year then as required	 Manage other vegetation and remove nuisance plants.
	Monthly for 6 months, quarterly for 2 years, then half yearly	Inspect vegetation coverage.
	Half yearly	 Inspect inlets and facility surface for silt accumulation, establish appropriate silt removal frequencies.
Occasional Maintenance	As required or if bare soil is exposed over > 10% of the swale treatment area	Reseed areas of poor vegetation growth, alter plant types to better suit conditions, if required.
Remedial Action	As required	 Repair erosion or other damage by re-turfing or reseeding; Relevel uneven surfaces and reinstate design levels; Scarify and spike topsoil layer to improve infiltration performance, break up silt deposits and prevent compaction of the soil surface; Remove build-up of sediment on upstream gravel trench, flow spreader or at top of filter strip; and Remove and dispose of oils or petrol residues using safe standard practices.

Table 4.2: The SuDS Manual Typical Maintenance Schedule for Detention Basins

Table 4.2: The s	subs Manual Typical <i>I</i>	Maintenance Schedule for Detention Basins
Maintenance Schedule	Typical Frequency	Required Action
Regular Maintenance	Monthly	 Remove litter and debris; Inspect inlets, outlets and overflows for blockages, and clear if required; and Inspect banksides, structures, pipework etc for evidence of physical damage.
	Monthly (during growing season, or as required	Cut grass – for spillways and access routes.
	Monthly for first year, then annually or as required	 Inspect inlets and facility surface for silt accumulation. Establish appropriate silt removal frequencies.
	Monthly at start, then as required	 Manage other vegetation and remove nuisance plants.
	Half yearly (spring – before nesting season, and autumn	Cut grass – meadow grass in and around basin.
	Annually	 Check any penstocks and other mechanical devices; Tidy all dead growth before start of growing season; and Manage wetland plants in outlet pool – where provided.
	Annually or as required	 Remove sediment from inlets, outlet and forebay.
Occasional Maintenance	As required	Reseed areas of poor vegetation growth.
	Every 2 years, or as required	Prune and trim any trees and remove cuttings.
	Every 5 years, or as required	Remove sediment from inlets, outlets, forebay and main basin when required.
Remedial Action	As required	 Repair/rehabilitation of inlets, outlets and overflows; and Relevel uneven surfaces and reinstate design levels.

Table 4.3: Typical Maintenance Schedule for the A42 Inlet Headwall

Maintenance Schedule	Typical Frequency	Required Action		
Regular Maintenance	Monthly	 Undertake inspection of grating to ensure it is securely fixed without blockages. 		
	Monthly (during growing season)	Strim vegetation 1m min. surround to structures and keep hard aprons free from silt and debris.		
	Annually, after major storm event, or as required	 Inspect surface structures removing obstructions and silt as necessary. Check there is no physical damage 		
	As required	Undertake inspection of headwall after leaf fall in autumn.		
Occasional Maintenance	As required	 Repair physical damage if necessary. Remove and dispose of oils or petrol residues using safe standard practices. 		
Monitoring	Monthly / after large storm events	Inspect structures for evidence of poor operation.		
	Half yearly	 Inspect silt accumulation rates and establish appropriate removal, frequencies. 		

5. FOUL WATER DRAINAGE

- 5.1 Foul water will be drained from the proposed development separately to surface water.
- 5.2 Based on level constraints within the site and the location of the nearby public sewerage infrastructure, foul flows from the entire development cannot drain via gravity. Therefore, it is proposed that foul flows will be collected and conveyed through the development towards a Type 3 pumping station, to be located towards the southern extent of the development.
- 5.3 It is proposed to pump flows back through the development to the north and into the existing foul public sewer network located within the A453 in the northwest site boundary. An alternative foul outfall is within the EMIA land to the east of the proposed site access point.
- 5.4 A pre-development enquiry with STW (**Appendix 9**) anticipates that the local sewerage network does not currently have capacity to accept flows from the proposed development and hydraulic modelling is required to determine what improvements to the network are necessary.
- 5.5 Discussions are ongoing with STW confirm the foul water solution for the proposed development. The latest correspondence is included within **Appendix 9**.
- 5.6 The final foul outfall location is to be confirmed; however, a proposed pumping station and potential outfall locations are illustrated on the Conceptual Drainage Strategy within **Appendix 6**.

6. SUMMARY

- 6.1 This statement and supporting appendices demonstrate that the drainage design for the development will comply with the relevant local and national standards, specifically the hierarchy of discharge, runoff rate and volume criterion.
- 6.2 This SDS is intended to support a DCO and as such the level of detail included is commensurate and subject to the nature of the proposals.

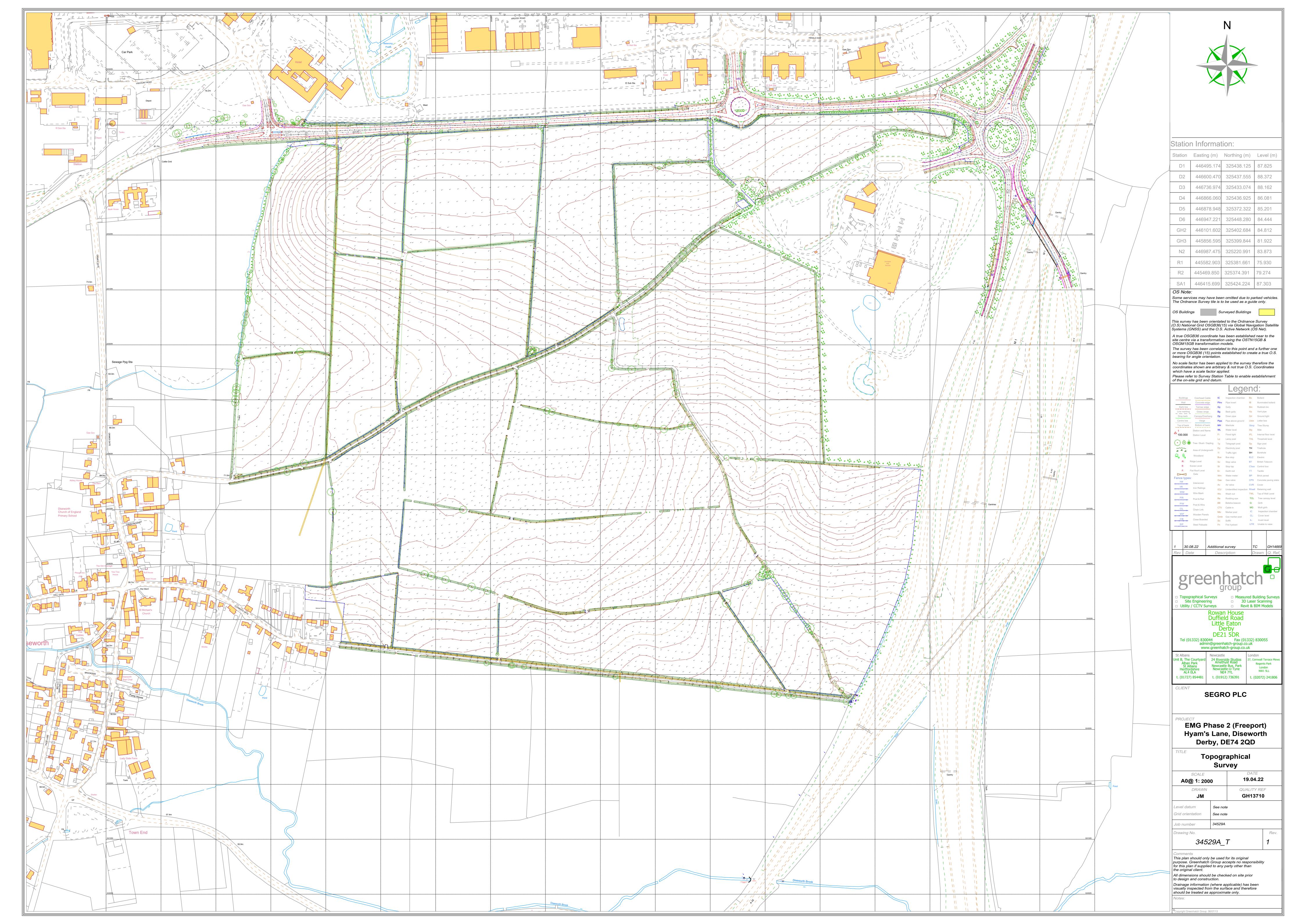
Table 6.1: Sustainable Drainage Statement Summary

lable 6.	able 6.1: Sustainable Drainage Statement Summary								
		Existing Site	Proposed Development						
Approx	mate Site Area (Ha)	104 (a _l	oprox.)						
Impermeable Area (Ha)		0	69.08 (approx.)						
Outfall I	ocation	Watercourse	Watercourse						
	1 in 1-Year	186.5							
f	QBAR	228.0							
Peak Runoff Rate (I/s)	1 in 30-Year	455.9	114.4						
eak Rate	1 in 100-Year	580.3							
	1 in 100-Year + CC	-							
Volume	Control	-	Discharge rate limited below QBAR						
Propose	ed Storage Volume	-	59,270m³						
Flow Co	ntrol Type	-	Vortex						
SuDS Features		-	Detention Basins, Swales and Downstream Defender						
Mainter	nance Responsibility	-	Management Company						

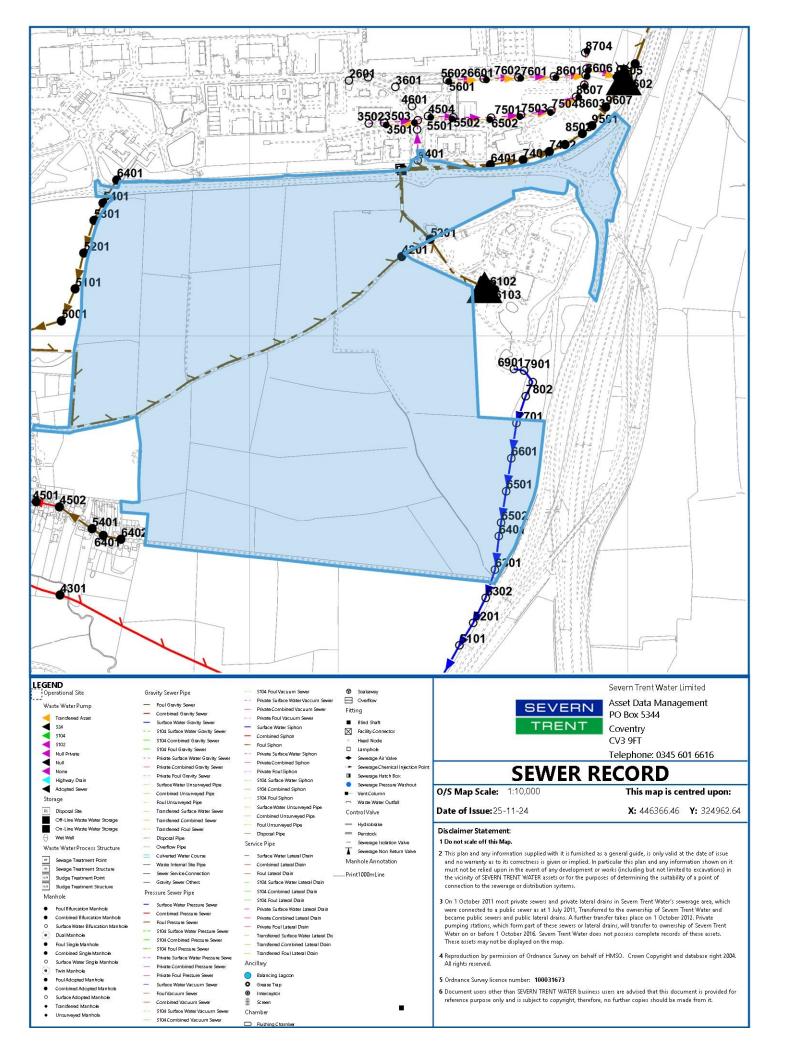
6.3 It is envisaged that the final drainage strategy will be determined during the detailed design stage, as the development layout is finalised.

APPENDICES

Appendix 1: Topographical Survey



Appendix 2: Sewer Asset Records



Sewer Node Sewer Pipe Data

Reference	Cover Level	Invert Level Upstream	Invert Level Downstream	Purpose	Material	Pipe Shape	Max Size	Min Size	Gradient	Year Laid
SK46238704	49.185	47.76	47.48	S	CO	С	525	<unk></unk>	57.71	31/12/1899 00:00:00
SK46246501	69.188	66.45	63.58	S	СО	С	375	<unk></unk>	29.31	31/12/1899
SK46259608	81.716	80.09	<unk></unk>	F	VC	С	300	<unk></unk>	0.35	00:00:00 31/12/1899 00:00:00
SK46258702	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46244001	56.3829	54.65	54.67	S	СО	С	375	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
SK46255602	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	450	<unk></unk>	0	31/12/1899 00:00:00
SK46239706	50.45	49.52	48.93	S	СО	С	300	<unk></unk>	23.05	31/12/1899 00:00:00
SK46254501	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46258501	91.01	88.72	85.49	F	VC	С	300	<unk></unk>	16.41	31/12/1899 00:00:00
SK46239704	50.525	48.9	48.668	С	СО	С	<unk></unk>	<unk></unk>	<unk></unk>	17/01/2022 00:00:00
SK45255401	73.564	70.564	70.477	F	VC	С	300	<unk></unk>	577.44	31/12/1899 00:00:00
SK45255001	69.938	68.038	67.704	F	VC	С	300	<unk></unk>	356.36	31/12/1899 00:00:00
SK46254502	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46254505	<unk></unk>	<unk></unk>	<unk></unk>	S	со	С	450	<unk></unk>	0	31/12/1899 00:00:00
SK45243504	59.2299	57.46	57.18	С	VC	С	225	<unk></unk>	13.39	31/12/1899 00:00:00
SK46247801	87.207	83.77	83.05	S	СО	С	375	<unk></unk>	57.58	31/12/1899 00:00:00
SK46256502	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46255501	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46258601	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46259603	80.16	<unk></unk>	<unk></unk>	F	<unk></unk>	С	300	<unk></unk>	0	31/12/1899 00:00:00
SK47231703	50.8499	48.15	48.174	С	СО	С	<unk></unk>	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
SK46254201	<unk></unk>	<unk></unk>	<unk></unk>	F	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK46239701	49.2449	47.68	44.98	S	СО	С	600	<unk></unk>	39.51	31/12/1899 00:00:00
SK46254401	<unk></unk>	<unk></unk>	<unk></unk>	S	VC	С	300	<unk></unk>	0	31/12/1899 00:00:00
SK46246401	63.02	60.58	58.58	S	СО	С	375	<unk></unk>	45.06	31/12/1899 00:00:00
SK47231701	50.844	48.154	47.92	С	СО	С	<unk></unk>	<unk></unk>	351.78	31/12/1899 00:00:00
SK46245101	57.1629	55.62	55.18	S	СО	С	375	<unk></unk>	228.91	31/12/1899 00:00:00
SK46256103	<unk></unk>	<unk></unk>	88.34	F	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK46238702	52.235	49.32	49.09	С	СО	С	<unk></unk>	<unk></unk>	339.83	31/12/1899 00:00:00
SK47232701	51.22	47.9	47.765	С	СО	С	<unk></unk>	<unk></unk>	603.43	31/12/1899 00:00:00
SK45255201	71.732	69.532	68.964	F	VC	С	300	<unk></unk>	171.81	31/12/1899 00:00:00
SK45253001	68.804	67.704	63.25	F	VC	С	<unk></unk>	<unk></unk>	22.29	31/12/1899 00:00:00
SK46246302	59.6199	57.49	56.78	S	СО	С	375	<unk></unk>	102.99	31/12/1899 00:00:00
SK46258701	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46245001	56.3079	55.16	54.71	S	СО	С	375	<unk></unk>	196.53	31/12/1899 00:00:00
SK45245401	65.3399	63.31	61.51	F	VC	С	150	<unk></unk>	58.03	31/12/1899 00:00:00
SK46238703	52.095	50.44	47.73	S	СО	С	525	<unk></unk>	13.14	31/12/1899 00:00:00
SK47231704	50.895	48.5	48.2	С	СО	С	<unk></unk>	<unk></unk>	196.83	31/12/1899 00:00:00
SK46253501	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46258603	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK47233701	50.71	47.76	47.51	С	СО	С	<unk></unk>	<unk></unk>	301.16	31/12/1899 00:00:00

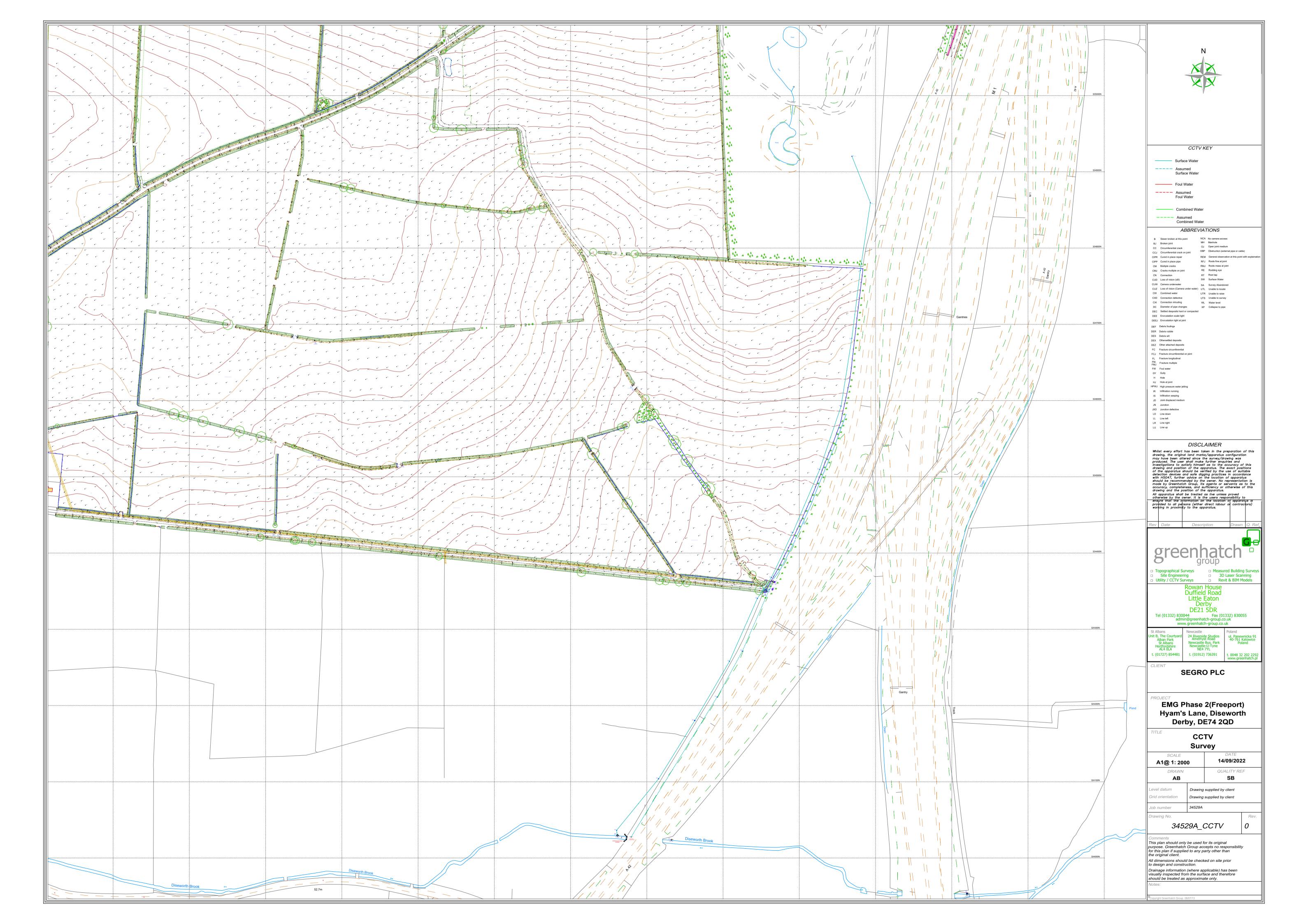
Sewer Node Sewer Pipe Data

- Jewel Tipe Buttu										
Reference	Cover Level	Invert Level Upstream	Invert Level Downstream	Purpose	Material	Pipe Shape	Max Size	Min Size	Gradient	Year Laid
SK46257401	<unk></unk>	<unk></unk>	90.62	F	VC	С	<unk></unk>	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
SK46259607	83.6419	81.74	80.12	F	VC	С	300	<unk></unk>	34.57	31/12/1899 00:00:00
SK46258704	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46257501	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46255502	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46256102	93.1679	88.33	87.63	F	VC	С	225	<unk></unk>	19.51	31/12/1899 00:00:00
SK45246402	66.2699	64.41	64.02	F	VC	С	150	<unk></unk>	123.13	31/12/1899 00:00:00
SK46258608	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	750	<unk></unk>	0	31/12/1899 00:00:00
SK46258607	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46245201	58.755	56.78	55.66	S	СО	С	375	<unk></unk>	62.32	31/12/1899 00:00:00
SK46257402	92.5179	90.58	88.77	F	VC	С	300	<unk></unk>	24.86	31/12/1899 00:00:00
SK46258502	87.8349	85.49	83.93	F	VC	С	300	<unk></unk>	20.51	31/12/1899 00:00:00
SK46256601	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46246502	65.302	63.54	60.6	S	СО	С	375	<unk></unk>	12.57	31/12/1899 00:00:00
SK46259602	80.16	<unk></unk>	<unk></unk>	F	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK46253502	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	375	<unk></unk>	0	31/12/1899 00:00:00
SK45255301	73.177	70.477	69.532	F	VC	С	300	<unk></unk>	95.53	31/12/1899 00:00:00
SK45244301	55.0999	<unk></unk>	<unk></unk>	С	PE	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK46257602	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46246301	60.332	58.56	57.5	S	СО	С	375	<unk></unk>	74.13	31/12/1899 00:00:00
SK45244501	61.7599	59.75	57.48	С	VC	С	225	<unk></unk>	36.22	31/12/1899 00:00:00
SK46255601	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46256602	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	525	<unk></unk>	0	31/12/1899 00:00:00
SK46258605	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46254503	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	525	<unk></unk>	0	31/12/1899 00:00:00
SK46258604	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK45246401	65.3499	64.01	63.32	F	VC	С	150	<unk></unk>	49.86	31/12/1899 00:00:00
SK47250701	80.0309	<unk></unk>	88.8	F	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK46257502	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46259606	80.16	<unk></unk>	<unk></unk>	F	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00
SK46246901	85.5559	84.43	84.21	S	СО	С	375	<unk></unk>	126.36	31/12/1899 00:00:00
SK46258602	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46256501	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46254504	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46257503	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
SK46259501	86.0569	83.9	81.76	F	VC	С	300	<unk></unk>	28.97	31/12/1899 00:00:00
SK46247802	84.507	82.91	76.01	S	со	С	375	<unk></unk>	10.91	31/12/1899 00:00:00
SK46259605	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46258703	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	1200	<unk></unk>	0	31/12/1899 00:00:00
SK46258606	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	1200	<unk></unk>	0	31/12/1899 00:00:00
SK46246601	72.0059	69.76	66.49	S	СО	С	375	<unk></unk>	26.93	31/12/1899 00:00:00
SK46255201	99.359	97.94	<unk></unk>	F	PVC	<unk></unk>	<unk></unk>	<unk></unk>	0	31/12/1899 00:00:00

Sewer Node Sewer Pipe Data

Reference	Cover Level	Invert Level Upstream	Invert Level Downstream	Purpose	Material	Pipe Shape	Max Size	Min Size	Gradient	Year Laid
SK46256401	95.2419	93.64	<unk></unk>	F	VC	С	300	<unk></unk>	0.93	31/12/1899 00:00:00
SK46239703	50.805	49.08	48.91	С	СО	С	<unk></unk>	<unk></unk>	276.53	31/12/1899 00:00:00
SK46239702	30.43	27.71	47.75	s	СО	С	600	<unk></unk>	<unk></unk>	31/12/1899 00:00:00
SK46253503	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	450	<unk></unk>	0	31/12/1899 00:00:00
SK45255101	70.8639	68.964	68.038	F	VC	С	300	<unk></unk>	99.44	31/12/1899 00:00:00
SK46247901	86.9759	84.2	83.81	S	СО	С	375	<unk></unk>	95.85	31/12/1899 00:00:00
SK47230700	<unk></unk>	48.668	48.51	С	СО	С	<unk></unk>	<unk></unk>	<unk></unk>	17/01/2022 00:00:00
SK46257601	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	С	225	<unk></unk>	0	31/12/1899 00:00:00
SK46247701	77.507	74.86	69.81	S	СО	С	375	<unk></unk>	18.46	31/12/1899 00:00:00
SK45256401	74.7939	70.794	70.564	F	VC	С	300	<unk></unk>	307.52	31/12/1899 00:00:00
SK45244502	63.33	61.46	59.76	С	VC	С	150	<unk></unk>	35.89	31/12/1899 00:00:00
SK46257504	<unk></unk>	<unk></unk>	<unk></unk>	S	СО	С	600	<unk></unk>	0	31/12/1899 00:00:00
<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	F	VC	<unk></unk>	<unk></unk>	<unk></unk>	<unk></unk>	01/12/2020 00:00:00

Appendix 3: CCTV Survey







CCTV Drainage Survey

East Midlands Gateway, Longholden.

CCTV DRAINAGE SURVEY REPORT















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Project Name	Project Number	Project Date
site	1	30/08/2022

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SectionItem3: MH04 > MH01 (MH04X)	5
Section Item 4: MH05 > MH04 (MH05X)	7
Section Item 5: MH03 > MH06 (MH03X)	9
SectionItem6: MH06 > MH07 (MH06X)	11
Section Item 7: MH07 > MH08 (MH07X)	12
Section Item 8: MH08 > MH09 (MH08X)	14
SectionItem9: MH09 > MH10 (MH09X)	16
Section Item 10: MH11 > MH12 (MH11X)	18
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14B Orgreave Close, Sheffield Tel. 0114 251 3481 info@sewersurveysuk.co.uk

Project Information

Project Name	Project Number	Project Date
site	1	30/08/2022

Client

Company: Greenhatch Group
Contact: Adam Sneddon
Department: Associate Director

Street: Rowan House, Duffield Road

Town or City: Little Eaton, Derby

Post Code: DE21 5DR **Phone:** 01332 830044

Email: utilities@greenhatch-group.co.uk

Site

Contact: Adam Sneddon

Department: Associate Director

Street: East Midlands Gateway

Town or City: Longholden **Phone:** 01332 830044

Email: utilities@greenhatch-group.co.uk

Contractor

Company: Sewer Surveys UK Ltd

Contact: Andrew Froggatt/ Simon Bennett

Department: Directors

Street: 14B Orgreave Close

Town or City: Sheffield **Post Code:** S13 9NP

Phone: 0114 251 3481

Mobile: 07837 768649/07808 220160 Email: info@sewersurveysuk.co.uk

site P-1

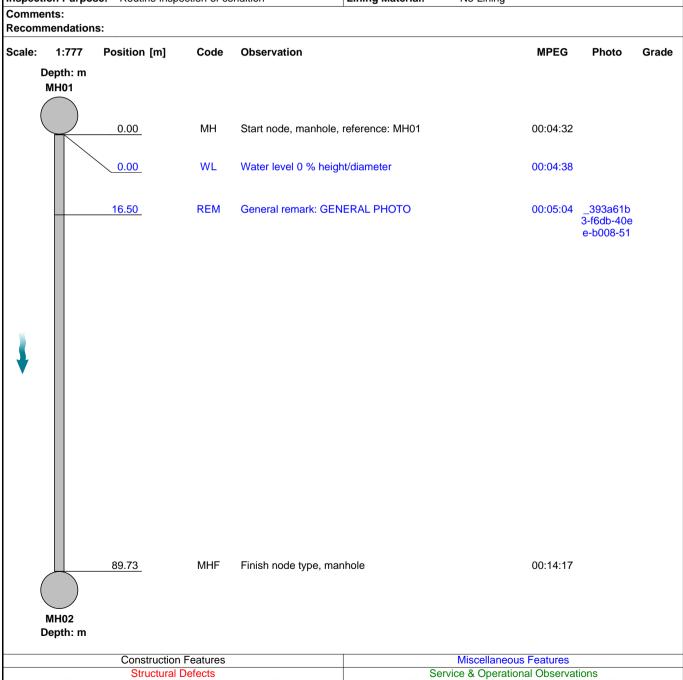


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Section Inspection - 06/09/2022 - MH01X

				•			
Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
1	1	06/09/22	15:16	1	No Rain Or Snow	Not Specified	MH01X
Operator		Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
S	BY	YR67	VYO	Forward View	Not Specified	Not Specified	1

Town or Village:		Inspection Direction:	Downstream	Upstream Node NAMS Re MH01
Road:	Long Holden (Off)	Inspected Length:	89.73 m	Upstream Pipe Depth:
Location:		Total Length:	89.73 m	Downstream Node NAMS Ref: MH02
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of condition		Lining Material:	No Lining



	Con	struction Feat	ures		Miscellaneous Features				
Structural Defects					Service & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0 0.0 0.0 0.0				



Section Pictures - 06/09/2022 - MH01X

Section	Inspection Direction	PLR	Client`s Job Ref	Contractor`s Job Ref
1	Downstream	MH01Y	1	



_393a61b3-f6db-40ee-b008-516be3f87a8c.jpg, 00:05:04, 16.50 m General remark, GENERAL PHOTO



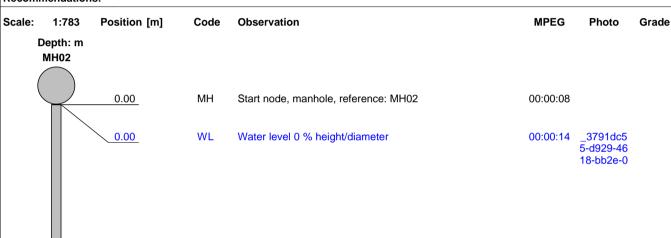
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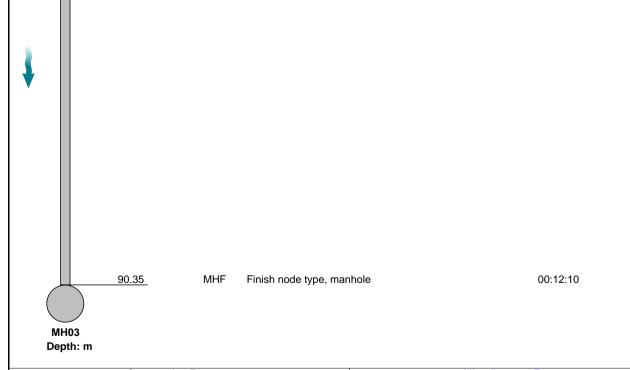
Section Inspection - 06/09/2022 - MH02X

				-			
Section	Inspection	Date	Time	Client's Job Ref	Weather	Pre Cleaned	PLR
2	1	06/09/22	15:16	1	No Rain Or Snow	Not Specified	MH02X
Operator		Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
S	BY	YR67	'VYO	Forward View	Not Specified	Not Specified	2

Town or Village: Upstream Node NAMS Re MH02 Inspection Direction: Downstream **Upstream Pipe Depth:** Road: Long Holden (Off) Inspected Length: 90.35 m Location: **Total Length:** 90.35 m Downstream Node NAMS Ref: MH03 Surface Type: Joint Length: 2.50 m **Downstream Pipe Depth:** Use: Surface water Pipe Shape: Type of Pipe: Dia/Height: 450 mm Flow Control: Pipe Material: Concrete Not Specified Year Constructed: **Lining Type:** No Lining Inspection Purpose: Routine inspection of condition **Lining Material:** No Lining Comments: WRONG SIZE ON RECORDING

Recommendations:





	Construction Features					Miscellaneous Features			
	Structural Defects					Service & Operational Observations			
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0 0.0 0.0 0.0 1.0					0.0	0.0	0.0	1.0



Section Pictures - 06/09/2022 - MH02X

Section	Inspection Direction	PLR	Client`s Job Ref	Contractor`s Job Ref
2	Downstream	MH02X	1	



_3791dc55-d929-4618-bb2e-0e758fedf0dd.jpg, 00:00:14, 0.00 m
Water level 0 % height/diameter



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Section Inspection - 06/09/2022 - MH04X

Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
3	1	06/09/22	15:16	1	No Rain Or Snow	Not Specified	MH04X
Ope	rator	Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
S	BY	YR67	'VYO	Forward View	Not Specified	Not Specified	3

Town or Village:		Inspection Direction:	Upstream	Upstream Node NAMS Re MH04
Road:	Long Holden (Off)	Inspected Length:	89.04 m	Upstream Pipe Depth:
Location:		Total Length:	89.04 m	Downstream Node NAMS Ref: MH01
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water	•	Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of	condition	Lining Material:	No Lining
Comments:			1	
-				

cale:	1:771	Position [m]	Code	Observation	MPEG	Photo	Grade
	Pepth: m MH01						
(0.00	МН	Start node, manhole, reference: MH04	00:00:08		
		0.00	WL	Water level 0 % height/diameter	00:00:16		
		1.64	CN	Connection at 06 o'clock, dia 350 mm: BACKDROP	00:01:16		
		30.07	GP	General Condition photograph	00:05:17	_65dd77e 6-3518-4a e3-b96e-6	
1							
	MH04 Pepth: m	89.04	MHF	Finish node type, manhole	00:12:26		
_	opun m			Miscellane			

STR No. Def STR Peak STR Mean STR Total STR Grade SER No. Def SER Peak SER Mean SER Total SER Grade 0.0 0.0 0.0 1.0 0.0 0.0 0.0 0 0 1.0



Section Pictures - 06/09/2022 - MH04X

Section	Inspection Direction	PLR	Client's Job Ref	Contractor`s Job Ref
3	Unstream	MHOAX	1	



_65dd77e6-3518-4ae3-b96e-6d0e2b6ca48d.jpg, 00:05:17, 30.07 m General Condition photograph

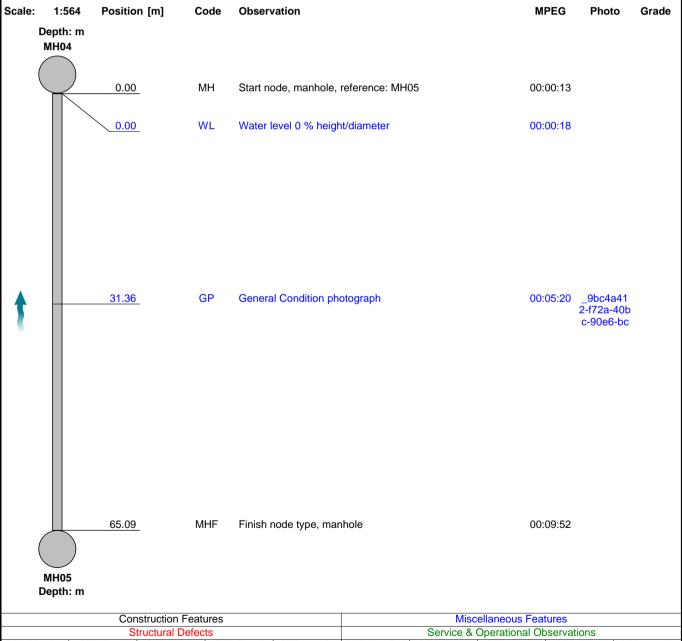


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Section Inspection - 06/09/2022 - MH05X

				-			
Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
4	1	06/09/22	15:17	1	No Rain Or Snow	Not Specified	MH05X
Ope	rator	Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
S	BY	YR67	'VYO	Forward View	Not Specified	Not Specified	4

Town or Village:		Inspection Direction:	Upstream	Upstream Node NAMS Re MH05
Road:	Long Holden (Off)	Inspected Length:	65.09 m	Upstream Pipe Depth:
Location:		Total Length:	65.09 m	Downstream Node NAMS Ref: MH04
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	C
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of condition		Lining Material:	No Lining
Comments:			-	-



	Structural Defects					Service & Operational Observations SER No. Def SER Peak SER Mean SER Total SER Grade			
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def SER Peak SER Mean SER Total SER Grade				SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0



Section Pictures - 06/09/2022 - MH05X

Section	Inspection Direction	PLR	Client`s Job Ref	Contractor`s Job Ref
4	Unstream	MH05X	1	



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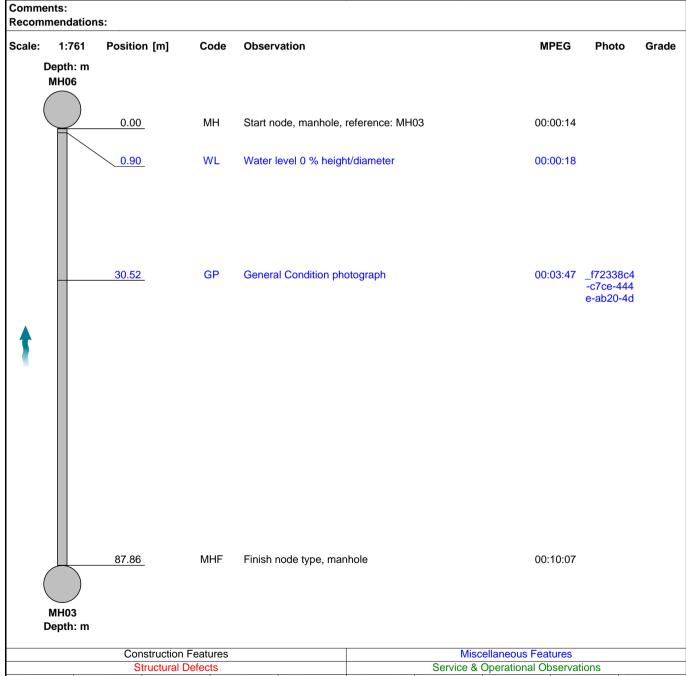


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Section Inspection - 06/09/2022 - MH03X

				-			
Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
5	1	06/09/22	15:17	1	No Rain Or Snow	Not Specified	MH03X
Ope	erator	Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
S	BY	YR67	'VYO	Forward View	Not Specified	Not Specified	5

Town or Village:		Inspection Direction:	Upstream	Upstream Node NAMS Re MH03
Road:	Long Holden (Off)	Inspected Length:	87.86 m	Upstream Pipe Depth:
Location:		Total Length:	87.86 m	Downstream Node NAMS Ref: MH06
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of condition		Lining Material:	No Lining
Comments:				
Recommendations:				

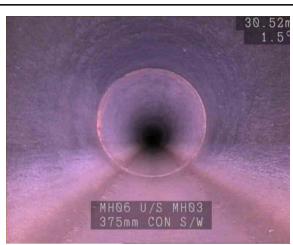


	00.	ion donon i odio	2100			111100	onarioodo i odi	aroo	I I
	S	tructural Defec	ts			Service & 0	Operational Ob	servations	
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0



Section Pictures - 06/09/2022 - MH03X

Section	Inspection Direction	PLR	Client`s Job Ref	Contractor`s Job Ref
5	Unstream	MH03X	1	



_f72338c4-c7ce-444e-ab20-4d2f6b493fe3.jpg, 00:03:47, 30.52 m General Condition photograph

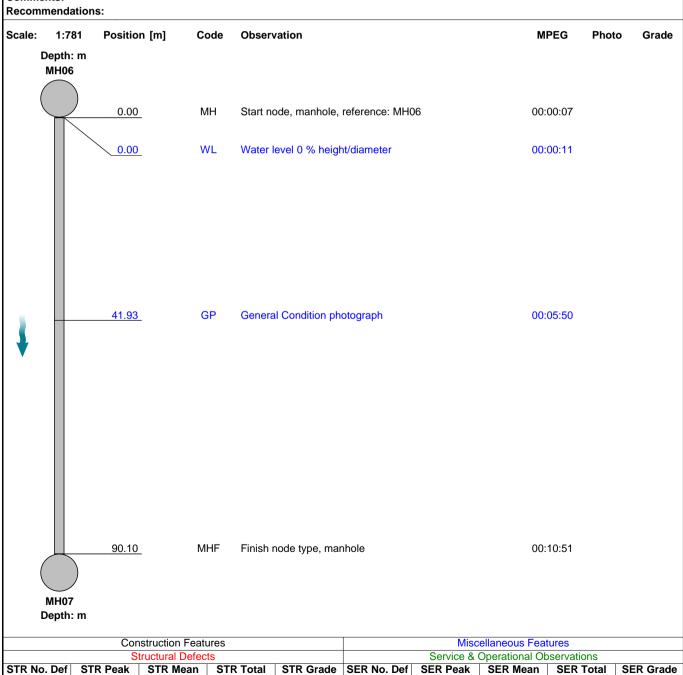


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Section Inspection -	06/09/2022 - MH06X
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Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
6	1	06/09/22	15:17	1	No Rain Or Snow	Not Specified	MH06X
Ope	rator	Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
S	BY	YR67	VYO	Forward View	Not Specified	Not Specified	6

Town or Village:		Inspection Direction:	Downstream	Upstream Node NAMS Re MH06
Road:	Long Holden (Off)	Inspected Length:	90.10 m	Upstream Pipe Depth:
Location:		Total Length:	90.10 m	Downstream Node NAMS Ref: MH07
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of o	condition	Lining Material:	No Lining
Comments: Recommendations:			1	



site 11

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				=			
Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
7	1	06/09/22	15:17	1	No Rain Or Snow	Not Specified	MH07X
Ope	rator	Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
SI	BY	YR67	VYO	Forward View	Not Specified	Not Specified	7

Town or Village:		Inspection Direction:	Downstream	Upstream Node NAMS Re MH07
Road:	Long Holden (Off)	Inspected Length:	65.27 m	Upstream Pipe Depth:
Location:		Total Length:	65.27 m	Downstream Node NAMS Ref: MH08
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water	-	Pipe Shape:	C
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of	condition	Lining Material:	No Lining
Comments:			1	
Recommendations:				

Comme Recomr	ents: mendatior	is:						
Scale:	1:566	Position [m]	Code	Observation		MPEG	Photo	Grade
	Depth: m MH07							
(0.00	МН	Start node, manhole,	reference: MH07	00:00:41		
		0.01	WL	Water level 5 % heigh	nt/diameter	00:00:43		
		<u> 15.15</u>	GP	General Condition ph	otograph	00:02:51	_47d42bd 8-e68a-4e 2a-90c6-4	
\		32.95	GP	General Condition ph	otograph	00:05:07	_3078535 5-44ad-45 cd-aeeb-8	
		54.13	GP	General Condition ph	otograph	00:07:36	_68d97c0 9-de87-40 1e-bf68-54	
(65.27	MHF	Finish node type, mar	nhole	00:09:09		
	MH08 Depth: m							
		Construction Structural I			Se	Miscellaneous Features rvice & Operational Observat	ions	

	Cor	struction Feat	ures			Misc	ellaneous Feat	tures		
	Structural Defects					Service & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade	
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0	



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Section Pictures - 06/09/2022 - MH07X

 Section
 Inspection Direction
 PLR
 Client`s Job Ref
 Contractor`s Job Ref

 7
 Downstream
 MH07X
 1



_47d42bd8-e68a-4e2a-90c6-400fcb21c963.jpg, 00:02:51, 15.15 m General Condition photograph



_30785355-44ad-45cd-aeeb-84b5ac5cf1b2.jpg, 00:05:07, 32.95 m

General Condition photograph



_68d97c09-de87-401e-bf68-5477b2e16760.jpg, 00:07:36, 54.13 m General Condition photograph



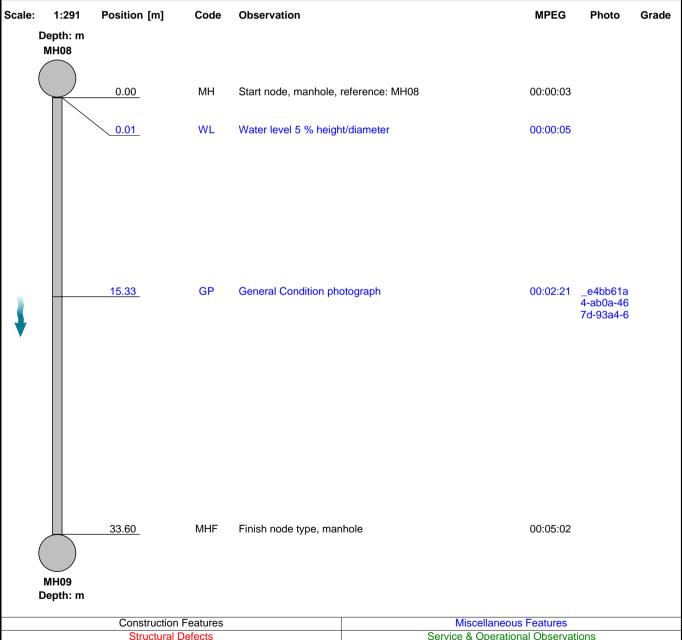
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Section Inspection - 06/09/2022 - MH08X

				-			
Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
8	1	06/09/22	15:17	Not Specified	No Rain Or Snow	Not Specified	MH08X
Ope	rator	Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
S	BY	YR67	VYO	Forward View	Not Specified	Not Specified	8

Town or Village:		Inspection Direction:	Downstream	Upstream Node NAMS Re MH08
Road:	Long Holden (Off)	Inspected Length:	33.60 m	Upstream Pipe Depth:
Location:		Total Length:	33.60 m	Downstream Node NAMS Ref: MH09
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of	condition	Lining Material:	No Lining
Comments:	•		1	
Dagammandations				

Recommendations:



	O	il detalal Delec	13		Oct vice & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0



Section Pictures - 06/09/2022 - MH08X

Section	Inspection Direction	PLR	Client`s Job Ref	Contractor`s Job Ref
8	Downstream	MHOSX		



_e4bb61a4-ab0a-467d-93a4-65bbdad6d939.jpg, 00:02:21, 15.33 m General Condition photograph

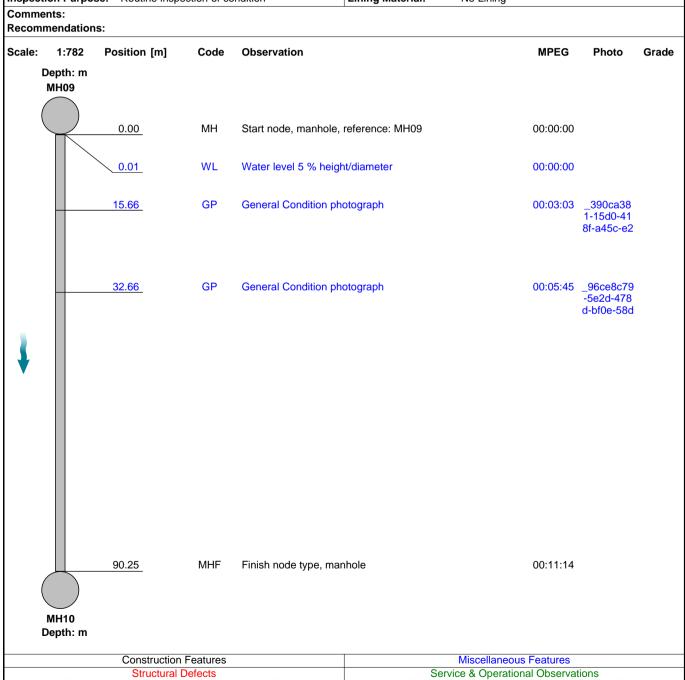


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Section Inspection - 06/09/2022 - MH09X

				-				
Section	Inspection	ection Date Time		Client`s Job Ref Weather		Pre Cleaned	PLR	
9	1	06/09/22	15:17	Not Specified	No Rain Or Snow	Not Specified	MH09X	
Operator		Veh	icle	Camera	Preset Length	Legal Status	NAMS ID	
SBY				Forward View Not Specified		Not Specified	9	

Town or Village:		Inspection Direction:	Downstream	Upstream Node NAMS Re MH09
Road:	Long Holden (Off)	Inspected Length:	90.25 m	Upstream Pipe Depth:
Location:		Total Length:	90.25 m	Downstream Node NAMS Ref: MH10
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of condition		Lining Material:	No Lining
Comments:				



	Cor	struction Feat	ures		Miscellaneous Features				
	S	tructural Defec	ts		Service & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0



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Section Pictures - 06/09/2022 - MH09X

 Section
 Inspection Direction
 PLR
 Client's Job Ref
 Contractor's Job Ref

 9
 Downstream
 MH09X



_390ca381-15d0-418f-a45c-e2b560419aa3.jpg, 00:03:03, 15.66 m General Condition photograph



_96ce8c79-5e2d-478d-bf0e-58d48171529f.jpg, 00:05:45, 32.66 m

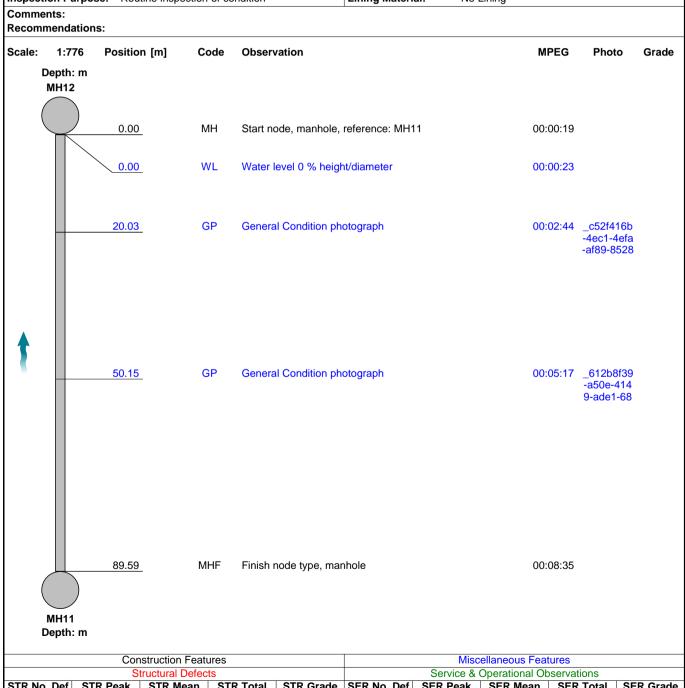
General Condition photograph



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				•						
Section	Inspection	spection Date Time		Client`s Job Ref Weather		Pre Cleaned	PLR			
10	1	06/09/22	15:17	Not Specified	No Rain Or Snow	Not Specified	MH11X			
Оре	Operator		icle	Camera	Preset Length	Legal Status	NAMS ID			
SBY		YR67 VYO		Forward View Not Specified		Not Specified	10			

Town or Village:		Inspection Direction:	Upstream	Upstream Node NAMS Re MH11
Road:	Long Holden (Off)	Inspected Length:	89.59 m	Upstream Pipe Depth:
Location:		Total Length:	89.59 m	Downstream Node NAMS Ref: MH12
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of condition		Lining Material:	No Lining
Comments:			1	
Decemmendations				



	Structural Defects				Service & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0



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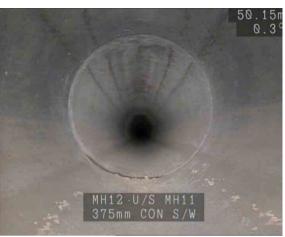
Section Pictures - 06/09/2022 - MH11X

 Section
 Inspection Direction
 PLR
 Client's Job Ref
 Contractor's Job Ref

 10
 Upstream
 MH11X



_c52f416b-4ec1-4efa-af89-8528181f16d6.jpg, 00:02:44, 20.03 m General Condition photograph



_612b8f39-a50e-4149-ade1-68436daa23fc.jpg, 00:05:17, 50.15 m

General Condition photograph

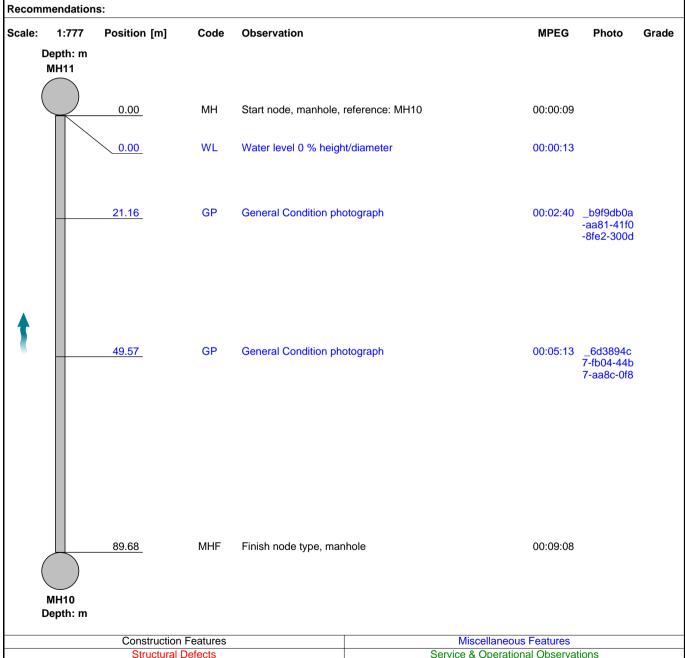


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Section Inspection - 06/09/2022 - MH10X

Section	Inspection	Date Time		ime Client's Job Ref Weather		Pre Cleaned	PLR
11	11 1 06/09/22 15:18		Not Specified	No Rain Or Snow	Not Specified	MH10X	
Operator		Vehicle		Camera	Preset Length	Legal Status	NAMS ID
SBY		YR67	VYO	Forward View	Not Specified	Not Specified	11

Town or Village:		Inspection Direction:	Upstream	Upstream Node NAMS Re MH10
Road:	Long Holden (Off)	Inspected Length:	89.68 m	Upstream Pipe Depth:
Location:		Total Length:	89.68 m	Downstream Node NAMS Ref: MH11
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of condition		Lining Material:	No Lining
Comments:				
Docommondations				



	Con	struction Feat	ures		Miscellaneous Features				
	S	tructural Defec	ts		Service & Operational Observations				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0



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Section Pictures - 06/09/2022 - MH10X

Section Inspection Direction PLR Client`s Job Ref Contractor`s Job Ref
11 Upstream MH10X



_b9f9db0a-aa81-41f0-8fe2-300d445328ad.jpg, 00:02:40, 21.16 m General Condition photograph



_6d3894c7-fb04-44b7-aa8c-0f877416d629.jpg, 00:05:13, 49.57 m

General Condition photograph



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Section Inspection -	06/09/2022 - MH12X
----------------------	--------------------

Section	Inspection	n Date Time		Client`s Job Ref	Weather	Pre Cleaned	PLR	
12	1	06/09/22	15:18	Not Specified	No Rain Or Snow	Not Specified	MH12X	
Operator		Vehicle		Camera	Preset Length	Legal Status	NAMS ID	
SBY		YR67 VYO		Forward View	Not Specified	Not Specified	12	

Town or Village:			Inspection Direction:	Downstream	Upstream Node NAMS	Re MH12		
Road:	Long Holden (Off) Inspected Length:			86.73 m	Upstream Pipe Depth:			
Location: Surface Type:			Total Length:	Downstream Node NAMS I	eam Node NAMS Ref: MH13			
			Joint Length:	2.50 m	Downstream Pipe Depth:			
Use:	Surface wate	r		Pipe Shape:	С			
Type of Pipe:				Dia/Height:	375 mm			
Flow Control:				Pipe Material:	Concrete			
Year Constructed: Not Specified				Lining Type:	No Lining			
Inspection Purpose: Routine inspection of			ondition	Lining Material:	No Lining			
Comments: Recommendations:								
Scale: 1:751 Po	osition [m]	Code	Observation		MPEG	Photo	Grade	
Depth: m MH12								
	0.00	МН	Start node, manhole,	reference: MH12	00:00:07			
	0.00	WL	Water level 0 % heigh	ht/diameter	00:00:11			



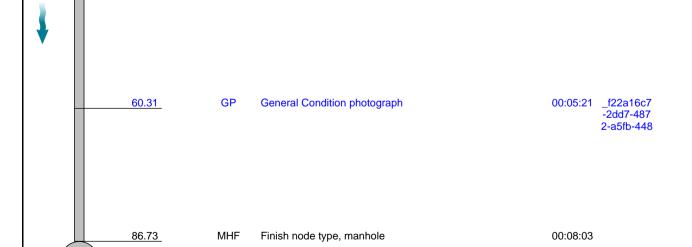
MH13

0.0

0.0

0.0

00:02:50 _03a2ace 7-3884-44 ee-9bcc-2



Depth	: m								
Construction Features					Miscellaneous Features				
Structural Defects				Service & Operational Observations					
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade

0

0.0

0.0

1.0

0.0

site 22

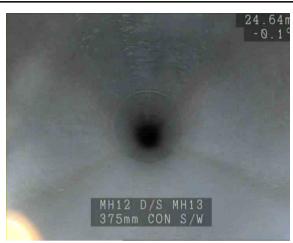
1.0



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Section Pictures - 06/09/2022 - MH12X

Section	Inspection Direction	PLR	Client's Job Ref	Contractor`s Job Ref
12	Downstream	MH12X		



_03a2ace7-3884-44ee-9bcc-249d12e54f09.jpg, 00:02:50, 24.64 m General Condition photograph



_f22a16c7-2dd7-4872-a5fb-448f33d4f7f3.jpg, 00:05:21, 60.31 General Condition photograph



Sewer Surveys UK Ltd

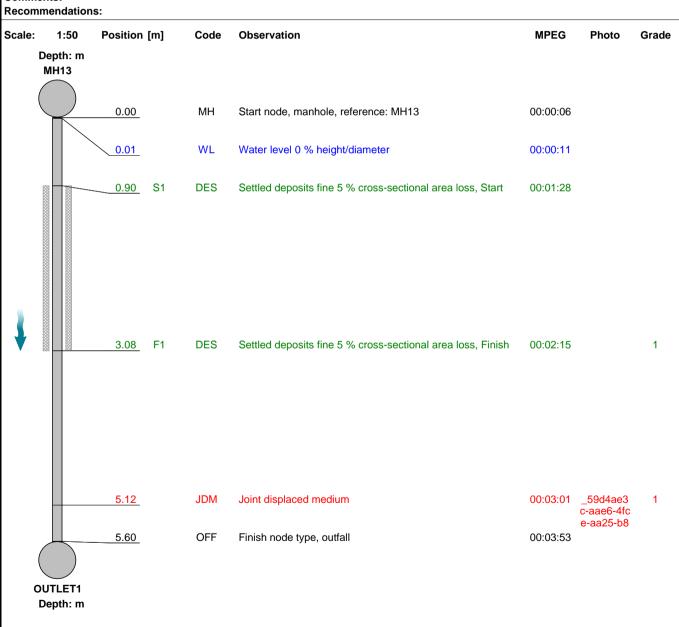
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Section Inspection - 31/08/2022

Section	Inspection	Date	Time	Client`s Job Ref	Weather	Pre Cleaned	PLR
13	1	31/08/22	14:56	Not Specified	No Rain Or Snow	Not Specified	Not Specified
Operator		Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
SBY		YR67	'VYO	Forward View	Not Specified	Not Specified	13

Town or Village:		Inspection Direction:	Downstream	Upstream Node NAMS Re MH13
Road:	Long Holden (Off)	Inspected Length:	5.60 m	Upstream Pipe Depth:
Location:		Total Length:	5.60 m	Downstream Node NAMS Ref: OUTLET1
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	375 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of condition		Lining Material:	No Lining

Comments:



Construction Features					Miscellaneous Features				
	S	tructural Defec	Defects Service & Operational Observations						
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
1	1.0	0.2	1.0	1.0	1	0.0	0.0	0.0	1.0



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Section Pictures - 31/08/2022

Section	Inspection Direction	PLR	Client`s Job Ref	Contractor`s Job Ref
13	Downstream			



_59d4ae3c-aae6-4fce-aa25-b87ad489547b.jpg, 00:03:01, 5.12 Joint displaced medium



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Section Inspection - 01/09/2022

Section	tion Inspection Date Time		Client`s Job Ref	Weather	Pre Cleaned	PLR	
14	1	01/09/22	8:22	Not Specified	No Rain Or Snow	Not Specified	Not Specified
Operator		Veh	icle	Camera	Preset Length	Legal Status	NAMS ID
SBY		YR67	'VYO	Forward View	Not Specified	Not Specified	14

Town or Village:		Inspection Direction:	Downstream	Upstream Node NAMS Re INLET
Road:	Long Holden (Off)	Inspected Length:	3.24 m	Upstream Pipe Depth:
Location:		Total Length:	3.24 m	Downstream Node NAMS Ref: MH14
Surface Type:		Joint Length:	2.50 m	Downstream Pipe Depth:
Use:	Surface water		Pipe Shape:	С
Type of Pipe:			Dia/Height:	525 mm
Flow Control:			Pipe Material:	Concrete
Year Constructed:	Not Specified		Lining Type:	No Lining
Inspection Purpose:	Routine inspection of	condition	Lining Material:	No Lining
Comments:			•	

Recommendations:

Depth: m

Scale:	1:50	Position [m]	Code	Observation	MPEG	Photo	Grade
	Depth: m INLET						
		0.00	OC	Start node, other special chamber, reference: INLET	00:00:07		
		0.90	WL	Water level 5 % height/diameter	00:00:14		
1		0.91 S1	DES	Settled deposits fine 5 % cross-sectional area loss, Start	00:00:27		
		3.24_ F1	DES	Settled deposits fine 5 % cross-sectional area loss, Finish	00:01:30		1
	MH14	3.24	MHF	Finish node type, manhole	00:01:58		

Construction Features					Miscellaneous Features					
	Structural Defects					Service & Operational Observations				
STR	No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def SER Peak SER Mean SER Total SER Gr				SER Grade
	0	0.0	0.0	0.0	1.0	1	0.0	0.0	0.0	1.0



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Section Profile

Project Name	Project Number	Project Date
site	1	30/08/2022

C, 375	mm						
Section	Upstream Node NAMS Ref	Downstream Node NAMS Ref	Date	Road	Pipe Material	Total Length	Inspected Length
1	MH01	MH02	06/09/2022	LONG HOLDEN (OFF)	Concrete	89.73 m	89.73 m
3	MH04	MH01	06/09/2022	LONG HOLDEN (OFF)	Concrete	89.04 m	89.04 m
4	MH05	MH04	06/09/2022	LONG HOLDEN (OFF)	Concrete	65.09 m	65.09 m
5	MH03	MH06	06/09/2022	LONG HOLDEN (OFF)	Concrete	87.86 m	87.86 m
6	MH06	MH07	06/09/2022	LONG HOLDEN (OFF)	Concrete	90.10 m	90.10 m
7	MH07	MH08	06/09/2022	LONG HOLDEN (OFF)	Concrete	65.27 m	65.27 m
8	MH08	MH09	06/09/2022	LONG HOLDEN (OFF)	Concrete	33.60 m	33.60 m
9	MH09	MH10	06/09/2022	LONG HOLDEN (OFF)	Concrete	90.25 m	90.25 m
10	MH11	MH12	06/09/2022	LONG HOLDEN (OFF)	Concrete	89.59 m	89.59 m
11	MH10	MH11	06/09/2022	LONG HOLDEN (OFF)	Concrete	89.68 m	89.68 m
12	MH12	MH13	06/09/2022	LONG HOLDEN (OFF)	Concrete	86.73 m	86.73 m
13	MH13	OUTLET1	31/08/2022	LONG HOLDEN (OFF)	Concrete	5.60 m	5.60 m

Total: 12 Inspections x C 375 mm = 882.54 m Total Length and 882.54 m Inspected Length

C, 450 mm

Section	Upstream Node NAMS Ref	Downstream Node NAMS Ref	Date	Road	Pipe Material	Total Length	Inspected Length
2	MH02	MH03	06/09/2022	LONG HOLDEN (OFF)	Concrete	90.35 m	90.35 m

Total: 1 Inspection x C 450 mm = 90.35 m Total Length and 90.35 m Inspected Length

C, 525 mm

Section	Upstream Node NAMS Ref	Downstream Node NAMS Ref	Date	Road	Pipe Material	Total Length	Inspected Length
14	INLET	MH14	01/09/2022	LONG HOLDEN (OFF)	Concrete	3.24 m	3.24 m

Total: 1 Inspection x C 525 mm = 3.24 m Total Length and 3.24 m Inspected Length

Total: 14 Inspections = 976.13 m Total Length and 976.13 m Inspected Length

site P-1



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Scoring Summary

Project Name	Project Number	Project Date
site	1	30/08/2022

Structural Defects

Section PLR Grade Description

All inspected pipes are in an acceptable structural condition (< grade 3).

Service / Operational Condition

Section PLR Grade Description

All inspected pipes are in an acceptable service condition (< grade 3).

Abandoned Surveys

Section PLR Description

All inspections complete, none are abandoned.

Information

These scoring summaries are based on the SRM grading from the WRc.

site P-1



Job	Num	ber:									Surve	у Ву:	SBY		
Grid	d Ref:				No	de	e Num	ber: N	ЛН01		Cove	er Lev	rel:		
Loc	ation:	East Mid	lands Ga	teway											
Yea	ır Laid	I: Z	Status: I	PU	Fund	tic	on: SV	/ Node	Type: M	IH	Surve	y Dat	e: 30/08/22		
Mar	nufact	urer:									Gratin	ıg:			
CC	VEF	Shape	: DT	Hinged	: / Lc	ck	(able:	/ Dut	y: M	Size:610	/610	Тох	ic atmos:		
SH	IAFT	Side I	Entry: /	Regula	ating C	οι	ırses:	4 Depth	n: 600	Size:60	00/600		Vermin:		
CF	IAME	SFR So	offit Type:	,] [No. of	St	ep Iro	ns: 6 N	lo. of La	dders:	No	o. of L	andings:		
		00/1200	Const'n					of Flow:		pth of Si			l of S:		
	Pipe U/S D/S node Reference Shape Pipe Size Backdrop Diameter Pipe Material Lining Material Depth from Cover (M) Invert Level (M)														
A MH04 C 375 CO 1.49															
SJAI	В														
MING	B C D D D														
INCO	D														
	E														
	F														
PIPES	Х	MH02		С	375				СО	1	2.	67			
교	Y														
		CONDITI		⊥ DRM∆TI	ON	Fr	nter V	if attentio	n require	ad IIsa	Remarl	cs to c	clarify		
	С	over	Irons/La		Sł			Chamb		Benching		Other			
Rei	marks	::													
					i.				14						
									1	A					
											1	C			
			和意义								7				
	\														
										X	1				



Job	Num	ber:									Survey By	: SBY		
Gric	d Ref:				No	de l	Num	ber: N	/IH02		Cover Le	vel:		
Loc	ation:	East Mid	lands Ga	teway										
Yea	ır Laid	I: Z	Status:	PU	Func	tion	: SW	Node	Туре: М	Н	Survey Da	te: 30/08/22		
Mar	nufact	urer:									Grating:			
CC	OVEF	Shape	: DT	Hinged	l: / Lc	cka	ble: /	/ Dut	y: M	Size:620)/620 To	xic atmos:		
SH	IAFT	Side I	Entry: /	Regul	ating C	ours	ses:	5 Depth	n: 680	Size:6	00/600	Vermin:		
CH	IAME	BER So	offit Type:	1	No. of	Step	o Iror	ns: 5 N	o. of La	dders:	No. of I	_andings:		
Siz	It:	H of S:												
Pipe U/S D/S node Reference Shape Pipe Size Backdrop Diameter Pipe Material Lining Material Depth from Cover (M) Invert Leve (M) A MH01 C 375 CO 2.20														
	Α	MH01		2.20										
INCOMING PIPES	В			-										
MING	С													
INCO	D													
-	Е													
	F													
PIPES	X	MH03		С	375				СО		2.26			
		CONDITI	ON INFO) RMATI	ION	Ente	er Y i	f attention	n require	ed. Use	Remarks to	clarify		
	С	over	Irons/La			aft		Chamb		Benchin		<u> </u>		
Rei	marks	»:												



Job	Numl	ber:										Sur	vey By	: SBY
Grid	d Ref:					No	de N	lumb	er: N	иН03		Со	ver Le	vel:
Loc	ation:	East Mid	lands Ga	teway										
Yea	ar Laid	l: Z	Status:	PU	Fu	ınci	tion:	SW	Node	Туре:	МН	Surv	vey Da	te: 30/08/22
Mar	nufact	urer:										Gra	ting:	
CC	OVER	Shape	: DT	Hinged	d: /	Lo	ckat	ole:/	Dut	y: M	Size:610	610	To	xic atmos:
SH	IAFT	Side I	Entry: /	Regul	ating	g Co	ours	es: 2	Depth	ո։ 450	Size:60	00/60	0	Vermin:
CH	HAME	BER So	offit Type:	/	No.	of S	Step	Iron	s: 7 N	lo. of L	_adders:		No. of I	Landings:
Siz	e: 120	00/1200	Const'n	Code:	СО		Dep	th of	Flow:		Depth of Si	lt:		H of S:
	Pipe	U/S D/S Refer		Shape	ı	Pipe	Size		Backdrop Diameter	Pipe Materia		Dep Co	oth from ver (M)	Invert Level (M)
	Α	MH02		С	37	5				СО		2	2.70	
INCOMING PIPES	В													
MING	С													
INCO	D													
	E													
	F													
PIPES	Х	MH06		С	37	5				СО			2.73	
<u> </u>	Υ													
ι		CONDITI	ON INFO	RMAT	ION	E	nte	r Y if	attentio	n requ	ired. Use	Rema	arks to	clarify
	C	over	Irons/La	dders		Sh			Chamb		Benching		Othe	
Re	marks	:												
											A			
					<u> </u>									
			1		i a							1	C	
													CL	
										1				
											X	1	4	



Job	Num	ber:									Survey	y By:	SBY		
Gric	d Ref:				No	ode	e Num	ber: N	ин06		Cove	r Lev	rel:		
Loc	ation:	East Mid	lands Ga	teway											
Yea	ır Laic	I: Z	Status:	PU	Fund	ctic	on: SW	/ Node	Туре: М	IH	Survey	/ Dat	e: 30/08/22		
Mar	nufact	urer:									Grating	j :			
CC	OVEF	Shape	: DT	Hinged	l: / Lo	ck	kable:	/ Dut	ty: M	Size:610	/610	Тох	ic atmos:		
SH	IAFT	Side	Entry: /	Regul	ating C	οι	ırses:	2 Depth	n: 450	Size:6	00/600		Vermin:		
CH	IAME	BER So	offit Type:	/	No. of	St	ep Iro	ns: 3	lo. of La	dders:	No.	of L	andings:		
Siz	e: 120	00/1200	Const'n	Code:	СО	D	epth o	of Flow:	De	pth of Si	lt:		l of S:		
	Pipe U/S D/S node Reference Shape Pipe Size Backdrop Diameter Pipe Material Lining Material Depth from Cover (M) Invert Level (M) A MH03 C 375 CO 1.73														
NCOMING PIPES	В														
OMING	С														
INCO	D														
	E														
	F														
PIPES	X	MH07		С	375				СО		1.7	5			
<u> </u>	Y														
		CONDITI	ION INFO	RMAT	ION	Er	nter Y	if attentio	n require	ed. Use	Remark	s to c	clarify		
	С	over	Irons/La	dders	Sł	naf	ft	Chamb	er	Benchin	g C	Other			
Rei	marks);													
			The same of the sa	and the second								75			
										A					
									50	-		F			
											E	1			
											1	7			
										1	19	1			
			-24		X.					V					



Job	Num	ber:									Surve	у Ву:	SBY
Grid	d Ref:				No	de	Numb	er: I	MH07		Cove	er Lev	/el:
Loc	ation:	East Mid	lands Ga	ateway									
Yea	ar Laic	I: Z	Status:	PU	Fund	ctic	n: SW	Node	Type: I	МН	Surve	y Dat	e: 30/08/22
Mai	nufact	urer:									Gratin	g:	
CC	OVEF	Shape	: DT	Hinged	d: / Lo	ck	able: /	Du	ty: M	Size:610	/610	Tox	ic atmos:
SH	IAFT	Side I	Entry: /	Regul	ating C	οι	ırses: 2	Deptl	h: 480	Size:6	00/600		Vermin:
CH	HAME	BER So	ffit Type	:/	No. of	St	ep Iron	s: 3 N	lo. of L	adders:	No	o. of L	.andings:
Siz	e: 135	50/1350	Constin	Code:	СО	D	epth of	f Flow:	D	epth of Si	ilt:	F	l of S:
	Pipe	U/S D/S Refere		Shape	Pip	e S	ize	Backdrop Diameter	Pipe Materia	Lining Il Material	Depth Cove		Invert Level (M)
	Α	MH06		С	375				СО		2.4	16	
NCOMING PIPES	В												
MING	С												
INCC	D												
	E												
	F												
PIPES	X	MH08		С	375				СО		2.4	48	
		CONDITI			ION	En	oter V if	attentio	n requi	red Use	Pemark	rs to r	clarify
	С	over	Irons/La			naf		Chamb		Benchin		Other	_
Re	marks):		·									
										A			
										$\bigvee_{\mathbb{X}}$	J		



Job	Num	ber:									Survey By	SBY
Grid	d Ref:				No	de	Num	ber: N	MH08		Cover Lev	/el:
Loc	ation:	East Mid	lands Ga	teway								
Yea	ar Laid	I: Z	Status: I	PU	Fund	tior	n: SW	Node	Туре: М	1H	Survey Dat	te: 31/08/22
Mai	nufact	urer:									Grating:	
CC	OVEF	Shape	: DT	Hinged	l: /	cka	able: /	/ Dut	y: M	Size:610/	(610 To)	cic atmos:
SH	HAFT	Side I	Entry: /	Regul	ating C	our	ses:	2 Depth	n: 470	Size:60	00/600	Vermin:
CH	HAME	BER So	offit Type:	/	No. of	Ste	p Iror	ns: 3 N	lo. of La	dders:	No. of L	andings:
		50/1350	Const'n	Code:	СО	De	epth c	of Flow:	De	pth of Sil	t: F	H of S:
	Pipe	U/S D/S Refere	Lining Material	Depth from Cover (M)	Invert Level (M)							
	Α	MH07		С	375				СО		1.74	
INCOMING PIPES	В											
MING	С											
INCO	D											
	Е											
	F											
S	X	MH09		С	375				СО		1.77	
PIPES	Υ											
,		CONDITI	ON INFO		IONI		V :	£ _##:_		- d	Dama aulea da	-1 - ::£ .
	С	CONDITI over	Irons/La			⊏nu naft		Chamb		Benching	Remarks to Othe	
Re	marks): ::										
										A		
					×						E	
		AR							Milos	X		



Job	Num	ber:											Sur	vey By	: SBY
Grio	d Ref:						No	de	Num	ber: N	иН09		Со	ver Le	/el:
Loc	ation:	East	Mid	lands Ga	iteway										
Yea	ır Laic	l: Z		Status:	PU	F	unc	tior	n: SW	Node	Type: I	ΜΗ	Sur	ey Dat	te: 31/08/22
Mar	nufact	urer:											Grat	ting:	
CC	OVEF	₹ Sh	ape	: SQ	Hinged	d: /	Lc	cka	able: /	/ Dut	ty: M	Size:620/	620	Тох	cic atmos:
SH	IAFT	S	ide	Entry: /	Regul	latin	g C	our	ses:	4 Depth	n: 640	Size:6	10/61	0	Vermin:
CH	IAME	BER	Sc	offit Type:	SL	No.	of	Ste	p Iror	ns: 4	lo. of L	adders:		No. of L	andings:
Siz	e: 135	50/135	0	Const'n	Code:	СО		De	pth c	of Flow: 5	D	epth of Sil	lt:	ŀ	H of S:
	Pipe U/S D/S node Reference Shape Pipe Size Diameter Backdrop Diameter Pipe Material Lining Material													oth from ver (M)	Invert Level (M)
	A MH8 C 375 CO													2.15	
PIPES	В														
MING	B C D D														
INCO	D														
	E														
	F														
ES	X	МН	10		С	37	75				СО			1.77	
PIPES	Υ														
L		CON	DITI	ON INFO	 DRMAT	ION		Ente	er Y i	f attentio	n reaui	red. Use I	Rema	arks to	clarifv
	С	over		Irons/La				naft	_	Chamb		Benching		Othe	
Rei	marks):													
												A			
														T	
												X			



Job	Num	ber:									Surve	эу Ву:	SBY	
Grid	d Ref:				No	de	Num	ber: N	ЛН10		Cov	er Lev	/el:	
Loc	ation:	East Midl	lands Ga	teway										
Yea	ır Laid	l: Z	Status: I	PU	Fund	tio	n: SW	Node	Type: N	1H	Surve	y Dat	te: 31/08/22	
Mar	nufact	urer:									Gratin	ıg:		
CC	VEF	Shape	: SQ	Hinged	: / Lo	ck	able: /	/ Dut	y: H	Size:620	/620	Тох	dic atmos:	
SH	IAFT	Side E	Entry: /	Regula	ating C	ou	ırses:	5 Depth	า:	Size:6	10/610		Vermin:	
CH	IAME	BER So	ffit Type:	SL	No. of	Ste	ep Iror	ns:3	lo. of La	dders:	No	o. of L	andings:	
Siz	Size: 1350/1350 Const'n Code: CO Depth of Flow: 5 Depth of Silt: H of S: Pipe U/S D/S node Shape Pipe Size Backdrop Pipe Lining Depth from Invert Level													
	Reference Diameter Material Material Cover (M) (M)													
	A MH9 C 375 CO 1.99													
PIPES	S B B													
OMING	B													
INCO	D													
	E													
	F													
PIPES	X	MH11		С	375				СО		2.	.01		
<u> </u>	Y													
į.		CONDITI						f attentio						
		over	Irons/La	dders	Sł	naf	t	Chamb	er	Benchin	g	Other		
Re	marks	:												
		Serve						X					A	



Job	Num	ber:									Surv	ey By:	SBY
Grid	d Ref:				No	ode N	Numb	per: N	ЛН11		Co	ver Lev	el:
Loc	ation:	East Mi	dlands Ga	teway									
Yea	ar Laic	I: Z	Status:	PU	Fund	ction	SW	Node	Type: M	IH	Surv	ey Dat	e: 31/08/22
Maı	nufact	urer:									Grat	ing:	
CC	OVEF	Shap	e:SQx2	Hinged	d: / Lo	ockal	ole: /	Dut	y: H	Size:690	690	Tox	ic atmos:
SH	AFT	Side	Entry: /	Regul	ating C	ours	ses: 2	2 Depth	n: 480	Size:13	300/7	50	Vermin:
CH	HAME	BER S	offit Type:	SL	No. of	Step	Iron	ıs:2 N	o. of La	dders:	<u> </u>	lo. of L	andings:
Siz	e: 135	50/1350	Const'n	Code:	СО	Dep	oth o	f Flow: 5	De	pth of Si	lt:	H	l of S:
	Pipe		/S node erence	Shape	Pip	e Size	•	Backdrop Diameter	Pipe Material	Lining Material		th from ver (M)	Invert Level (M)
	Α	MH10		С	375				СО		1	.53	
S B B													
B C C D D													
INCO	D												
	Е												
	F												
PIPES	X	MH12		С	375				CO			1.55	
		CONDI	LION INFO	 DRMAT	ION	Ente	r Y if	attention	n require	ed. Use	Rema	rks to d	clarify
	С	over	Irons/La			naft		Chamb		Benchin		Other	
Re	marks	5 :											
										120			
					# 14.4 Fresh Press				X				A



Job	Numl	ber:									Surv	еу Ву	: SBY		
Grid	d Ref:				No	de	e Num	ıber: N	ЛН12		Cov	er Le	vel:		
Loc	ation:	East Midl	lands Ga	teway											
Yea	ır Laid	l: Z	Status: I	PU	Fund	ctic	n: SV	V Node	Туре: М	Н	Surve	ey Da	te: 31/08/22		
Mar	nufact	urer:									Gratii	ng:			
CC	VEF	Shape	:SQ	Hinged	l: /	ck	able:	/ Dut	y: H	Size:750	/750	Tox	kic atmos:		
SH	IAFT	Side E	Entry: /	Regula	ating C	οι	ırses:	1 Depth	n:430	Size:7	60/760		Vermin:		
CH	CHAMBER Soffit Type:SL No. of Step Irons:1 No. of Ladders: No. of Landings: Size: 1350/1350 Const'n Code: CO Depth of Flow: 5 Depth of Site: H. of S:														
Siz	Size: 1350/1350 Const'n Code: CO Depth of Flow: 5 Depth of Silt: H of S: Pine LI/S D/S node Shape Pine Size Backdron Pine Lining Depth from Invert Level														
	Pipe U/S D/S node Reference Shape Pipe Size Backdrop Diameter Pipe Material Lining Material Depth from Cover (M) Invert Level (M)														
	A MH11 C 375 CO 1.15														
S B B															
B C C D D															
INCO	D										-				
-	E														
	F														
	X	MH13		С	375				СО		1	.18			
PIPES	Υ														
L		CONDITI	ON INFO	RMATI	ON	Er	iter Y	if attentio	n require	ed. Use	Remar	ks to	clarify		
	С	over	Irons/La	dders		naf		Chamb		Benchin		Othe	<u>-</u>		
Rei	marks	:													
			1	- 1 Y							10000				
	Remarks:														



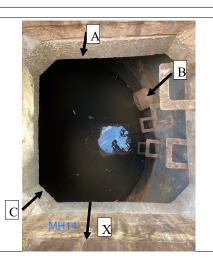
Job	Num	ber:										Su	ırvey By	: SBY	
Gric	d Ref:					No	de N	umb	er:	MH13		С	over Le	vel:	
Loc	ation:	East Mid	lands Ga	iteway											
Yea	ır Laid	I: Z	Status:	PU	Fu	ınc	tion:	SW	Node	Туре	: MH	Su	rvey Da	ite: 31/08/2	22
Mar	nufact	urer:										Gra	ating:		
CC	OVEF	Shape	:SQ	Hinge	d: /	Lo	ckab	le: /	Du	ty: H	Size:620	/620	То	xic atmos:	
SH	IAFT	Side	Entry: /	Regu	lating	j C	ourse	es: 5	Dept	h:700	Size:6	30/6	30	Vermin:	
CH	IAME	BER So	offit Type	:SL	No.	of :	Step	Iron	s: N	No. of	Ladders:		No. of	Landings:	
Siz	e: 135	50/1350	Const'n	Code:	СО		Dep	th of	Flow: 5		Depth of Si	ilt:		H of S:	
	Pipe	U/S D/S Refer		Shape	ı	Pip€	Size		Backdrop Diameter	Pipe Mater		De C	epth from cover (M)	Invert Lev (M)	vel
	Α	MH12		С	375	5				СО			1.71		
NCOMING PIPES	В														
MING	С														
INCO	D														
	E														-
-	F														
PIPES	Х	Outfall		С	37	5				СО)		1.74		
	Υ														
l		CONDITI	ION INFO	ORMAT	ION		Enter	Y if	attentio	n regi	uired. Use	Rem	narks to	clarify	
	С	over	Irons/La				aft		Chamb		Benchin		Othe		
Rei	marks	::													
										A		X †			



Job	Num	ber:									Surve	у Ву:	SBY
Gri	d Ref:				No	ode Nun	nber:	МН	14		Cove	er Lev	el:
Loc	cation	East Midl	ands Ga	teway									
Yea	ar Laid	d: Z	Status:	PU	Fund	ction: SV	V No	de Ty	pe: N	ИΗ	Surve	y Date	e: 31/08/22
Ма	Manufacturer: Grating:												
C	COVER Shape:DT Hinged: / Lockable: / Duty: M Size:610/610 Toxic atmos:												
Sł	SHAFT Side Entry: / Regulating Courses: 3 Depth:540 Size:600/600 Vermin:												
Cł	HAMI	BER So	ffit Type:		No. of	Step Iro	ns:6	No.	of La	adders:	No	o. of L	andings:
Siz	ze: 21	00/2100	Const'n	Code:	СО	Depth	of Flow	r:	De	epth of Sil	t:	Н	of S:
										Lining Material	Depth Cove		Invert Level (M)
	Α	Inlet1		С	525			(CO		1.7	77	
PIPES	В	Unknown		С	150			\	/C		1.4	46	
NCOMING PIPES	С	Inlet1		С	525			(CO		1.6	67	
NCO	D												
	E												
	F												
ES ES	X	Unknown		С	700			С	Ю		1.	93	
PIPES	Y												
		CONDITION	ON INFO	DRMAT	ION	Enter Y	if atter	ition re	equir	ed. Use l	Remark	ks to c	larify
	C	over	Irons/La	dders	SI	naft	Cha	mber		Benching	3	Other	

Remarks: Catchpit overall depth 2.20







Job	Job Number: Survey By: SBY												
Grid	d Ref:				1	lod	e Num	nber: I	MH15		Со	ver Lev	rel:
Loc	ation:	East Mid	lands Ga	teway									
Yea	ar Laic	l: Z	Status:	PU	Fu	nctio	on: SV	V Node	Type: M	1H	Surv	/ey Dat	e: 31/08/22
Mar	nufact	urer:									Grat	ting:	
CC	OVEF	Shape	:DT	Hinge	d: /	Locl	kable:	/ Du	ty: M	Size:610	/610	Тох	ic atmos:
SH	IAFT	Side I	Entry: /	Regu	lating	Co	urses:	1 Dept	h:370	Size:6	00/60	0	Vermin:
CH	HAME	BER So	ffit Type:		No. o	of St	ep Iro	ns:5	lo. of La	dders:	1	No. of L	andings:
Siz	e: 210	00/2100	Const'n	Code:	СО		epth o	of Flow:	De	pth of Si	lt:		l of S:
	Pipe	U/S D/S Refer		Shape	P	ipe S	Size	Backdrop Diameter	Pipe Material	Lining Material		oth from ver (M)	Invert Level (M)
	Α	MH14		С	525				СО			1.98	
INCOMING PIPES	В	Unknown		С	150				СО		1	1.75	
MING	С												
	E												
	F												
PIPES	X	MH16		С	700				СО			2.00	
' [CONDITI			ION	Er	nter V	if attentio	n require	ad Usa	Pema	arke to d	larify
	С	over	Irons/La			Sha		Chamb		Benchin		Other	
Re	marks	s:											
										A			В
										—			
									(K	1	
									/	. 1			
										\searrow	/	•	
										↓	,		
										\triangle	4		



Job	Num	ber:									Surve	еу Ву:	SBY
Grid	d Ref:				No	ode	Numb	per: I	MH16		Cove	er Lev	rel:
Loc	ation:	East Mid	lands Ga	ateway									
Yea	ar Laid	l: Z	Status:	PU	Fund	ction	n: SW	Node	Type: N	ИΗ	Surve	y Dat	e: 01/09/22
Ma	nufact	urer:									Gratin	ıg:	
CC	OVEF	Shape	:DT	Hinged	l: / Lo	ocka	able: /	Du	ty: M	Size:610/	7610 Toxic atmos:		
SH	HAFT	Side I	Entry: /	Regul	Regulating Courses: 2 Depth:450 Size:60								Vermin:
CH	НАМЕ	BER So	offit Type	: [No. of	Ste	p Iron	ns:5	No. of La	adders:	No	o. of L	andings:
Siz	e: 210	00/2100	Const'n	Code:	СО	De	epth o	f Flow:	De	epth of Si	lt:	H	l of S:
	Pipe	U/S D/S Refere		Shape	Pip	e Siz	ze	Backdrop Diameter	Pipe Material	Lining Material	Depth Cove	n from er (M)	Invert Level (M)
	Α	MH15		С	700				СО		1.9	98	
INCOMING PIPES	В												
MING	С												
NCO	D												
	E												
	F												
ES	Х	Brook		С	700				СО		2.	20	
PIPES	Y												
		CONDITI	ON INFO	ORMAT	ION	Ent	ter Y it	f attentio	n reauir	ed. Use	Remarl	ks to (clarify
	С	over	Irons/La			naft		Chamb		Benching		Other	
Re	marks	: Overall o	depth 2.3	32									
				NA									
										A	11-16		
				(IO) as									

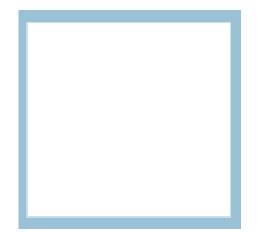


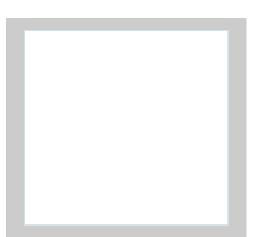
Cover Level: Survey Date: 01/09/22 Grating: Toxic atmos: Vermin: No. of Landings: ilt: H of S: Depth from Cover (M) Invert Level (M)
Grating: Toxic atmos: Vermin: No. of Landings: ilt: H of S: Depth from Invert Level
Grating: Toxic atmos: Vermin: No. of Landings: ilt: H of S: Depth from Invert Level
Toxic atmos: Vermin: No. of Landings: ilt: H of S: Depth from Invert Level
Vermin: No. of Landings: ilt: H of S: Depth from Invert Level
No. of Landings: ilt: H of S: Depth from Invert Level
ilt: H of S: Depth from Invert Level
Depth from Invert Level
Remarks to clarify
g Other
_

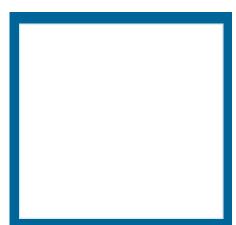


Job	Numl	ber:								Survey By	: SBY	
Grid	d Ref:				N	ode Nu	mber:	Outlet1		Cover Le	vel:	
Loc	ation:	East Mic	llands Ga	ateway								
Yea	ar Laid	I: Z	Status:	PU	Fun	ction: S	W	е Туре:	Outlet	Survey Da	te: 01/09/22	
Mar	nufact	urer:								Grating:		
CC	OVER	Shape	e :	Hinge	d: /	ockable	e: /	uty:	Size:	To	xic atmos:	
SH	IAFT	Side	Entry: /	Regul	lating (Courses	s: Dep	th:	Size:		Vermin:	
CH	HAME	BER S	offit Type	:	No. of	Step Ir	ons:	No. of L	adders:	No. of Landings:		
Siz	e:		Constin	Code:		Depth	of Flow:	D	epth of Sil	It: H of S:		
	Pipe		S node rence	Shape	Pip	e Size	Backdrop Diamete		Lining Material	Depth from Cover (M)	Invert Level (M)	
	Α											
NCOMING PIPES	В											
MING	С											
INCO	D											
	E											
	F											
PIPES	Х	mMH13		С	375			СО		1.22		
250 E	Y											
Į		CONDIT	ION INFO	ORMAT	ION	Enter \	∕ if attenti	on requi	red. Use I	Remarks to	clarifv	
	C	over	Irons/La			haft	Cham		Benching			
Re	marks):										
1												















Appendix 4: Greenfield Runoff Rate Calculations



Greenfield runoff rate estimation tool

hrwallingford www.uksuds.com | Greenfield runoff rate estimation tool (https://www.uksuds.com/)

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (CIRIA, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Project details

•	
Date	24/03/2025
Calculated by	Robin Green
Reference	EMG2
Model version	0.6.5

Location

Site name

Main Site

Site location

Diseworth



Site easting

Site northing

445919

324921

Site details

Total site area (ha)

1

### Display of the statistical in the statistical i	_				
My value 635 mm 640 QBar conversion 1.124 2.92	a	FEH statistical			
## (mm) ## (mu) ##	statistical				
HOST		My value		Map value	
1.124 2.92 1/4 2.92 1	·	635	mm		635
1.124 1.12	T	0.403			
2.32	QBar conversion	1.124			1.124
Owth curve factors Ological region ar growth factor 2 2-57 year growth factor 3.04 FEH statistical arate 1 year (l/s) arate 2 year (l/s) arate 10 years (l/s) Arate 30 years (l/s) Arate 30 years (l/s) Arate 30 years (l/s) Arate 30 years (l/s)	(I/s)	2.92	I/s		
My value 4 ar growth factor 2 2.57 year growth factor year growth factor 3.04 FEH statistical ar rate 1 year (I/s) ar rate 2 year (I/s) ar rate 30 years (I/s) 4 0.83 0.89 1.49 FEH statistical 2.7 1/s 4.9 1/s 4.9 1/s 4.9	FEH statistical) (I/s)	3.3	I/s		
My value 4	wth curve factors				
4	wth curve factors				
ar growth factor ar growth factor 0.89 1.49 2 2ear growth factor 3.04 FEH statistical arate 1 year (I/s) arate 2 year (I/s) 4.9 4.9 4.9 4.9 4.9 4.9	ogical ragion			Map value	
ar growth factor ar growth fa		4			4
par growth factor par growth factor par growth factor par growth factor 2.57 year growth factor 3.04 Sults and FEH statistical prate 1 year (l/s) prate 2 year (l/s) prate 10 years (l/s) 4.9 prate 30 years (l/s)		0.83			
pear growth factor 2	growth factor	0.89			
2.57	r growth factor	1.49			
Sults	r growth factor	2			
sults nod FEH statistical rate 1 year (I/s) 2.7 I/s rate 2 year (I/s) 2.9 I/s rate 10 years (I/s) 4.9 I/s	ar growth factor	2.57			
sults hod FEH statistical grate 1 year (I/s) 2.7 grate 2 year (I/s) 2.9 grate 10 years (I/s) 4.9 grate 30 years (I/s) 1/s	ar growth factor	3.04			
FEH statistical					
FEH statistical	ults				
2.7 1/s 2.7 1/s 2.9		FFH statistical			
rate 2 year (I/s) 2.9 1/s rate 10 years (I/s) 4.9 1/s	ate 1 year (I/s)		1/2		
rate 10 years (I/s) 4.9 rate 30 years (I/s)					
rate 30 years (I/s)			I/s		
rate ou years (I/S)			I/s		
0.0		6.6	I/s		
		8.4	l/s		
rate 200 years (I/s) 10	ate 200 years (I/s)	10	l/s		

 $responsibility \ of the \ users \ of \ this \ tool. \ No \ liability \ will \ be \ accepted \ by \ HR \ Walling ford, \ the \ Environment \ Agency, \ Centre \ for \ Ecology \ and \ Hydrology, \ Walling ford$

 $Hydrosolutions\ or\ any\ other\ organisation\ for\ the\ use\ of\ these\ data\ in\ the\ design\ or\ operational\ characteristics\ of\ any\ drainage\ scheme.$

Appendix 5: Greenfield Runoff Volume Calculation

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File: Main Site Concept Drainage Strategy_P4.

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Pre-development runoff volume

69.08ha

Simulation Settings

Rainfall Methodology FEH-22
Rainfall Events Singular
Summer CV 0.750

Winter CV 0.840
Analysis Speed Normal
Skip Steady State x

Drain Down Time (mins) 240 Additional Storage (m³/ha) 20.0 Starting Level (m)

Check Discharge Rate(s) x
Check Discharge Volume
√
100 year 360 minute (m³) 21232

Storm Durations

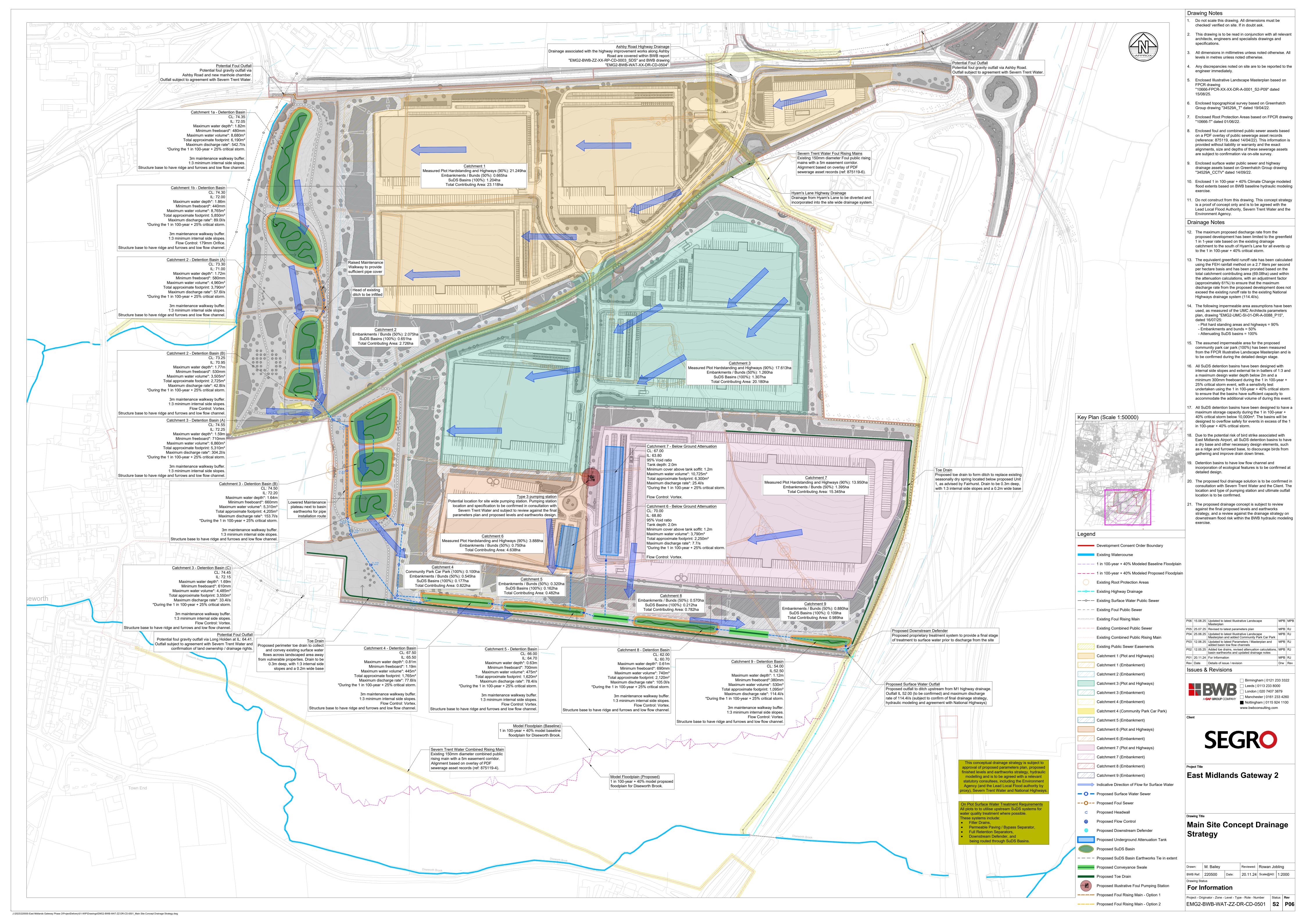
600 960 2160 10080 15 60 180 4320 7200 360 120 30 240 480 720 1440 2880 5760 8640

Return Period Climate Change Additional Area Additional Flow Return Period Climate Change Additional Area Additional Flow (CC %) (CC %) (A %) (A %) (years) (Q %) (years) (Q %) 25 0 40 0 100 100

Pre-development Discharge Volume

Cita Makaun	Croonfield	Soil Index	4	Datum Daried (veers)	100	Dottorment (0/)	0
Site Makeup	Greenneid	Soil maex	4	Return Period (years)	100	Betterment (%)	U
Greenfield Method	FSR/FEH	SPR	0.45	Climate Change (%)	0	PR	0.428
Positively Drained Area (ha)	69.080	CWI	95.852	Storm Duration (mins)	360	Runoff Volume (m³)	21232

Appendix 6: Concept Drainage Strategy



Appendix 7: Causeway Flow Calculations

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Outline Attenuation Calculations Ρ4

Design Settings

Rainfall Methodology FEH-22 Return Period (years) 100 Additional Flow (%) 0

CV 0.750 Time of Entry (mins) 5.00

Maximum Time of Concentration (mins) 30.00 Maximum Rainfall (mm/hr) 50.0 Minimum Velocity (m/s) 1.00 Connection Type Level Soffits Minimum Backdrop Height (m) 0.200

Preferred Cover Depth (m) 1.200 Include Intermediate Ground ✓ Enforce best practice design rules x

<u>Nodes</u>

	Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
Ca	tchment 1a	22.533	12.00	74.350		-92.158	100.836	2.300
Ca	tchment 1b	0.585	12.00	74.300		-93.671	70.218	2.300
Ca	tchment 2a	2.454	5.00	73.300		-92.916	37.295	2.300
Ca	tchment 2b	0.272	5.00	73.250		-92.626	22.671	2.300
Ca	tchment 3a	19.404	5.00	74.550		-65.281	7.280	2.300
Ca	tchment 3b	0.421	5.00	74.500		-65.281	-8.329	2.300
Ca	tchment 3c	0.355	5.00	74.450		-65.484	-22.137	2.300
Ca	tchment 4	0.822	5.00	67.500		-36.265	-57.268	2.000
Ca	tchment 5	0.482	5.00	66.000		-8.464	-60.549	1.300
Ca	tchment 6	4.638	5.00	70.000		1.763	-39.130	3.200
Ca	tchment 7	13.345	5.00	67.000		18.165	-40.189	3.200
Ca	tchment 8	0.782	5.00	62.000		29.356	-65.759	1.300
Ca	tchment 9	0.989	5.00	54.000		98.244	-74.249	1.650
2				53.000	1200	111.190	-87.933	0.967

<u>Links</u>

Name	US	DS	Length	ks (mm) /	US IL	DS IL	Fall	Slope	Dia	T of C	Rain
	Node	Node	(m)	n	(m)	(m)	(m)	(1:X)	(mm)	(mins)	(mm/hr)
1.000	Catchment 1a	Catchment 1b	30.000	0.600	72.050	72.000	0.050	600.0	600	12.51	0.0
2.000	Catchment 2a	Catchment 2b	24.000	0.600	71.000	70.950	0.050	480.0	600	5.36	50.0
1.000_1	Catchment 3a	Catchment 3b	24.000	0.600	72.250	72.200	0.050	480.0	600	5.36	50.0
1.001_1	Catchment 3b	Catchment 3c	23.900	0.600	72.200	72.150	0.050	478.0	600	5.72	50.0
4.000	Catchment 4	Catchment 5	32.500	0.600	65.500	64.700	0.800	40.6	365	5.19	50.0
5.000	Catchment 9	2	18.837	0.600	52.350	52.033	0.317	59.4	450	5.12	50.0
5.000	Catchinent 9	2	10.057	0.600	32.330	52.055	0.517	59.4	450	5.12	50.0

Name	Vel	Сар	Flow	US	DS	Σ Area	Σ Add	Pro	Pro
	(m/s)	(I/s)	(I/s)	Depth	Depth	(ha)	Inflow	Depth	Velocity
				(m)	(m)		(I/s)	(mm)	(m/s)
1.000	0.987	279.0	0.0	1.700	1.700	22.533	0.0	0	0.000
2.000	1.105	312.3	332.6	1.700	1.700	2.454	0.0	549	1.226
1.000_1	1.105	312.3	2629.7	1.700	1.700	19.404	0.0	600	1.114
1.001_1	1.107	313.0	2686.8	1.700	1.700	19.825	0.0	600	1.117
4.000	2.801	293.1	111.4	1.635	0.935	0.822	0.0	156	2.617
5.000	2.641	420.0	134.0	1.200	0.517	0.989	0.0	174	2.361

Pipeline Schedule

Link	Length	Slope	Dia	Link	US CL	US IL	US Depth	DS CL	DS IL	DS Depth
	(m)	(1:X)	(mm)	Type	(m)	(m)	(m)	(m)	(m)	(m)
1.000	30.000	600.0	600	Circular	74.350	72.050	1.700	74.300	72.000	1.700
2.000	24.000	480.0	600	Circular	73.300	71.000	1.700	73.250	70.950	1.700
1.000_1	24.000	480.0	600	Circular	74.550	72.250	1.700	74.500	72.200	1.700
1.001_1	23.900	478.0	600	Circular	74.500	72.200	1.700	74.450	72.150	1.700
4.000	32.500	40.6	365	Circular	67.500	65.500	1.635	66.000	64.700	0.935
5.000	18.837	59.4	450	Circular	54.000	52.350	1.200	53.000	52.033	0.517

Link	US	Node	DS	Dia	Node	MH		
	Node	Type	Node	(mm)	Type	Type		
1.000	Catchment 1a	Junction	Catchment 1b		Junction			
2.000	Catchment 2a	Junction	Catchment 2b		Junction			
1.000_1	Catchment 3a	Junction	Catchment 3b		Junction			
1.001_1	Catchment 3b	Junction	Catchment 3c		Junction			
4.000	Catchment 4	Junction	Catchment 5		Junction			
5.000	Catchment 9	Junction	2	1200	Manhole	Adoptable		

Manhole Schedule

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)
Catchment 1a	-92.158	100.836	74.350	2.300					
						Ů,	1.000	72.050	600

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Outline Attenuation Calculations P4

Manhole Schedule

			<u></u>	naminole s	, ci i c a a i c	_				
Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connection	ıs	Link	IL (m)	Dia (mm)
Catchment 1b	-93.671	70.218	74.300	2.300		1	1	1.000	72.000	600
Catchment 2a	-92.916	37.295	73.300	2.300		, , , , , , , , , , , , , , , , , , ,	0	2.000	71.000	600
Catchment 2b	-92.626	22.671	73.250	2.300		1	1	2.000	70.950	600
Catchment 3a	-65.281	7.280	74.550	2.300		,				
Catchment 3b	-65.281	-8.329	74.500	2.300		1	0	1.000_1 1.000_1	72.250 72.200	600 600
							0	1.001_1	72.200	600
Catchment 3c	-65.484	-22.137	74.450	2.300		1	1	1.001_1	72.200	600
Catchment 4	-36.265	-57.268	67.500	2.000		•→0				
Catchment 5	-8.464	-60.549	66.000	1.300		1	1	4.000	65.500 64.700	365 365
Catchment 6	1.763	-39.130	70.000	3.200		0				
Catchment 7	18.165	-40.189	67.000	3.200		o				
Catchment 8	29.356	-65.759	62.000	1.300		o				
Catchment 9	98.244	-74.249	54.000	1.650		~	0	5.000	52.350	450
2	111.190	-87.933	53.000	0.967	1200	1	1	5.000	52.033	450

Simulation Settings

Rainfall Methodology FEH-22 Rainfall Events Singular Summer CV 0.750			Winter Analysis Spe Skip Steady St		peed	eed Normal		Drain Down Time (Additional Storage (r Starting Lev		(m³/ha)	20.0	Check Discharge Rate(s) Check Discharge Volume 100 year 360 minute (m³)		x √ 21232			
									Stor	m Dı	urat	tions					
		15	6	0	180)	360		600	9	60	2160	4320	7200	10080		
		30	1	20	240)	480		720	14	140	2880	5760	8640			
Return Period (years)		e Change C %)			tional <i>i</i> (A %)			itior (Q	nal Flo %)		R	Return Period (years)		ate Change (CC %)	Additional Area (A %)	(0	onal Flow Q %)
100		25				C)			0		100		40	(i	0

Pre-development Discharge Volume

Site Makeup	Greenfield	Soil Index	4	Return Period (years)	100	Betterment (%)	0
Greenfield Method	FSR/FEH	SPR	0.45	Climate Change (%)	0	PR	0.428
Positively Drained Area (ha)	69.080	CWI	95.852	Storm Duration (mins)	360	Runoff Volume (m³)	21232

Node Catchment 1b Offline Orifice Control

Flap Valve	X	Invert Level (m)	72.000	Design Flow (I/s)	95.0	Discharge Coefficient	0.600
Loop to Node	Catchment 2a	Design Depth (m)	2.100	Diameter (m)	0.179		

Node Catchment 2b Offline ACO Q-Brake Control

Flap Valve	X	Invert Level (m)	70.950	Design Flow (I/s)	42.8	Min Node Diameter (mm)	1500
Loop to Node	Catchment 4	Design Depth (m)	2.200	Min Outlet Diameter (m)	0.295	Orifice Diameter (m)	0.234

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Outline Attenuation Calculations

Node Catchment 3c Offline ACO Q-Brake Control

Flap Valve x
Loop to Node Catchment 4

Invert Level (m) 72.150 Design Depth (m) 2.200 Design Flow (I/s) 33.4 Min Outlet Diameter (m) 0.220 Min Node Diameter (mm) 1500 Orifice Diameter (m) 0.210

Node Catchment 6 Offline ACO Q-Brake Control

Flap Valve x
Loop to Node Catchment 5

Invert Level (m) 66.800 Design Depth (m) 2.000

Design Flow (I/s) 7.7 Min Outlet Diameter (m) 0.145 Min Node Diameter (mm) 1050 Orifice Diameter (m) 0.110

Node Catchment 5 Offline Hydro-Brake® Control

Flap Valve x
Loop to Node Catchment 8
Invert Level (m) 64.700
Design Depth (m) 1.200

Design Flow (I/s) 78.4

Objective (HE) Minimise upstream storage

Sump Available

√

Product Number CTL-SHE-0354-7840-1200-7840

Min Outlet Diameter (m) 0.375 Min Node Diameter (mm) 2700

Node Catchment 7 Offline ACO Q-Brake Control

Flap Valve x Inv.
Loop to Node Catchment 8 Desi

Invert Level (m) 63.800 Design Depth (m) 2.000 Design Flow (I/s) 25.4 Min Outlet Diameter (m) 0.220 Min Node Diameter (mm) 1200 Orifice Diameter (m) 0.188

Node Catchment 8 Offline Hydro-Brake® Control

Flap Valve x
Loop to Node Catchment 9
Invert Level (m) 60.700
Design Depth (m) 1.200

Design Flow (I/s) 105.0
Objective (HE) Minimise upstream storage
Sump Available ✓

Product Number CTL-SHE-0400-1050-1200-1050

Min Outlet Diameter (m) 0.450 Min Node Diameter (mm) 3000

Node Catchment 4 Online ACO Q-Brake Control

Flap Valve x

Downstream Link 4.000

Replaces Downstream Link ✓

Invert Level (m) 65.500
Design Depth (m) 1.800
Design Flow (l/s) 77.6

Min Outlet Diameter (m) 0.365
Min Node Diameter (mm) 1800
Orifice Diameter (m) 0.314

Node Catchment 9 Online Hydro-Brake® Control

Flap Valve x
Downstream Link 5.000
Replaces Downstream Link √
Invert Level (m) 52.350
Design Depth (m) 1.200
Design Flow (l/s) 114.4

Objective (HE) Minimise upstream storage
Sump Available
Product Number CTL-SHE-0415-1144-1200-1144
Min Outlet Diameter (m) 0.450
Min Node Diameter (mm) 3000

Node Catchment 1a Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Side Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Porosity 1.00 Invert Level (m) 72.050 Time to half empty (mins)

Inf Area Inf Area Depth Area Depth Area (m²) (m) (m²)(m²)(m²)(m) 0.000 3533.5 0.0 2.300 6192.0 0.0

Node Catchment 1b Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Side Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Porosity 1.00 Invert Level (m) 72.000 Time to half empty (mins)

Depth Inf Area Area Inf Area Depth Area (m) (m²)(m²)(m) (m²) (m²)0.000 3932.0 0.0 2.300 5848.0 0.0

Node Catchment 2a Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Side Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Porosity 1.00 Invert Level (m) 71.000 Time to half empty (mins)

Depth Area Inf Area Depth Area Inf Area (m) (m²)(m²) (m²)(m²) (m) 3789.0 0.000 2305.0 0.0 2.300 0.0

Node Catchment 2b Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Side Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Porosity 1.00

Invert Level (m) 70.950 Time to half empty (mins)

Inf Area Inf Area Depth Area Depth Area (m²) (m) (m²)(m) (m²)(m²)0.000 1511.5 0.0 2.300 2723.5 0.0

Node Catchment 3a Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Side Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Porosity 1.00

Invert Level (m) 72.250
Time to half empty (mins)

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Outline Attenuation Calculations

Depth Area Inf Area Depth Inf Area Area (m) (m²) (m²) (m) (m²) (m²) 0.000 3543.0 2.300 5311.3 0.0

Node Catchment 3b Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 72.200 Side Inf Coefficient (m/hr) 0.00000 Porosity 1.00 Time to half empty (mins)

Depth Inf Area Depth Inf Area Area Area (m) (m²) (m²)(m) (m²) (m²)0.000 2704.4 0.0 2.300 4207.3 0.0

Node Catchment 3c Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 72.150 Side Inf Coefficient (m/hr) 0.00000 Porosity 1.00 Time to half empty (mins)

Depth Area Inf Area Depth Inf Area Area (m²)(m²)(m) (m²) (m) (m²) 0.000 2138.0 0.0 2.300 3551.7 0.0

Node Catchment 4 Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 65.500 Side Inf Coefficient (m/hr) 0.00000 Porosity 1.00 Time to half empty (mins) 0

 Depth
 Area (m)
 Inf Area (m²)
 Depth (m²)
 Area (m)
 Inf Area (m²)

 0.000
 229.6
 0.0
 2.000
 1765.8
 0.0

Node Catchment 5 Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 64.700 Side Inf Coefficient (m/hr) 0.00000 Porosity 1.00 Time to half empty (mins) 300

Depth Depth Inf Area Inf Area Area Area (m) (m²)(m²)(m²)(m²)(m) 0.000 471.1 1.300 1621.6 0.0 0.0

Node Catchment 6 Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 66.800 Side Inf Coefficient (m/hr) 0.00000 Porosity 0.95 Time to half empty (mins)

Depth Area Inf Area Depth Area Inf Area Depth Area Inf Area (m) (m²)(m²) (m) (m²)(m²)(m²)(m²) (m) 0.000 2240.0 0.0 2.000 2240.0 0.0 2.001 0.0 0.0

Node Catchment 7 Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 63.800 Side Inf Coefficient (m/hr) 0.00000 Porosity 0.95 Time to half empty (mins)

Depth Area Inf Area Depth Area Inf Area Depth Area Inf Area (m) (m²)(m²)(m) (m²)(m²)(m) (m²)(m²) 0.000 6300.0 0.0 2.000 6300.0 0.0 2.001 0.0 0.0

Node Catchment 8 Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 60.700 Side Inf Coefficient (m/hr) 0.00000 Porosity 1.00 Time to half empty (mins)

Depth Inf Area Area Depth Area Inf Area (m²)(m²) (m) (m²)(m) (m²)0.000 928.4 1.300 2120.6 0.0 0.0

Node Catchment 9 Depth/Area Storage Structure

Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 52.500 Side Inf Coefficient (m/hr) 0.00000 Porosity 1.00 Time to half empty (mins)

Depth Inf Area Area Inf Area Depth Area (m) (m²) (m²) (m) (m²) (m²) 1.500 1094.5 0.000 263.8 0.0 0.0

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Outline Attenuation Calculations P4

Results for 100 year +25% CC Critical Storm Duration. Lowest mass balance: 99.97%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
720 minute winter	Catchment 1a	705	73.866	1.816	1117.0	8679.7510	0.0000	SURCHARGED
720 minute winter	Catchment 1b	720	73.860	1.860	570.6	8764.9160	0.0000	ОК
7200 minute winter	Catchment 2a	7200	72.722	1.722	84.2	4961.2070	0.0000	SURCHARGED
7200 minute winter	Catchment 2b	7200	72.721	1.771	59.2	3507.1120	0.0000	OK
1440 minute winter	Catchment 3a	1440	73.837	1.587	520.9	6859.2290	0.0000	SURCHARGED
1440 minute winter	Catchment 3b	1440	73.837	1.637	315.5	5308.3870	0.0000	SURCHARGED
1440 minute winter	Catchment 3c	1440	73.837	1.687	163.2	4485.4600	0.0000	OK
720 minute winter	Catchment 4	675	66.312	0.812	109.3	446.0729	0.0000	SURCHARGED
1440 minute winter	Catchment 5	1440	65.329	0.629	90.1	475.6710	0.0000	OK
1440 minute winter	Catchment 6	1440	68.556	1.756	124.5	3787.5520	0.0000	OK
960 minute winter	Catchment 7	960	65.568	1.768	516.7	10727.3500	0.0000	OK
960 minute winter	Catchment 8	930	61.308	0.608	130.1	741.2571	0.0000	OK
720 minute winter	Catchment 9	705	53.467	1.117	152.3	527.8346	0.0000	SURCHARGED
15 minute summer	2	1	52.033	0.000	114.4	0.0000	0.0000	OK

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
720 minute winter	Catchment 1a	1.000	Catchment 1b	542.7	2.349	1.945	8.4503	
720 minute winter	Catchment 1b	Orifice	Catchment 2a	89.0				3535.9
7200 minute winter	Catchment 2a	2.000	Catchment 2b	57.5	1.095	0.184	6.7603	
7200 minute winter	Catchment 2b	ACO Q-Brake	Catchment 4	42.8				13204.0
1440 minute winter	Catchment 3a	1.000_1	Catchment 3b	304.2	1.669	0.974	6.7603	
1440 minute winter	Catchment 3b	1.001_1	Catchment 3c	153.7	1.692	0.491	6.7321	
1440 minute winter	Catchment 3c	ACO Q-Brake	Catchment 4	33.4				2383.2
720 minute winter	Catchment 4	ACO Q-Brake	Catchment 5	77.6				
1440 minute winter	Catchment 5	Hydro-Brake®	Catchment 8	78.4				5952.2
1440 minute winter	Catchment 6	ACO Q-Brake	Catchment 5	7.7				597.9
960 minute winter	Catchment 7	ACO Q-Brake	Catchment 8	25.4				1431.6
960 minute winter	Catchment 8	Hydro-Brake®	Catchment 9	105.0				5710.6
720 minute winter	Catchment 9	Hydro-Brake®	2	114.4				4939.7



File: Main Site Concept Drainage Strategy_P4. Network: Storm Network Matthew Bailey 24/07/2025

Page 6 EMG2

Outline Attenuation Calculations Ρ4

Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 99.97%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
720 minute winter	Catchment 1a	705	74.060	2.010	1251.2	9833.5180	0.0000	FLOOD RISK
720 minute winter	Catchment 1b	720	74.054	2.054	629.1	9841.9480	0.0000	OK
7200 minute winter	Catchment 2a	7260	72.890	1.890	90.5	5550.5210	0.0000	SURCHARGED
7200 minute winter	Catchment 2b	7260	72.890	1.940	61.2	3927.4440	0.0000	OK
1440 minute winter	Catchment 3a	1440	74.016	1.766	583.4	7754.9880	0.0000	SURCHARGED
1440 minute winter	Catchment 3b	1440	74.016	1.816	351.0	5995.3960	0.0000	SURCHARGED
1440 minute winter	Catchment 3c	1440	74.016	1.866	178.9	5064.2690	0.0000	OK
720 minute winter	Catchment 4	705	66.425	0.925	114.6	548.3627	0.0000	SURCHARGED
2160 minute winter	Catchment 5	1920	65.377	0.677	87.5	526.3657	0.0000	OK
1440 minute winter	Catchment 6	1440	68.784	1.984	139.4	4279.2080	0.0000	OK
1440 minute winter	Catchment 7	1440	65.794	1.994	401.2	12100.0800	0.0000	OK
960 minute winter	Catchment 8	960	61.379	0.679	132.6	849.5842	0.0000	OK
480 minute winter	Catchment 9	464	53.537	1.187	180.5	585.5822	0.0000	SURCHARGED
15 minute summer	2	1	52.033	0.000	114.4	0.0000	0.0000	OK

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
720 minute winter	Catchment 1a	1.000	Catchment 1b	597.9	2.355	2.143	8.4503	
720 minute winter	Catchment 1b	Orifice	Catchment 2a	93.8				3739.7
7200 minute winter	Catchment 2a	2.000	Catchment 2b	59.3	1.106	0.190	6.7603	
7200 minute winter	Catchment 2b	ACO Q-Brake	Catchment 4	42.8				13647.6
1440 minute winter	Catchment 3a	1.000_1	Catchment 3b	338.3	1.761	1.083	6.7603	
1440 minute winter	Catchment 3b	1.001_1	Catchment 3c	168.2	1.714	0.537	6.7321	
1440 minute winter	Catchment 3c	ACO Q-Brake	Catchment 4	33.4				2480.1
720 minute winter	Catchment 4	ACO Q-Brake	Catchment 5	77.6				
2160 minute winter	Catchment 5	Hydro-Brake®	Catchment 8	78.4				8606.3
1440 minute winter	Catchment 6	ACO Q-Brake	Catchment 5	7.7				626.0
1440 minute winter	Catchment 7	ACO Q-Brake	Catchment 8	25.4				2061.8
960 minute winter	Catchment 8	Hydro-Brake®	Catchment 9	105.0				5784.3
480 minute winter	Catchment 9	Hydro-Brake®	2	114.4				3914.8

East Midlands Gateway 2, Diseworth Sustainable Drainage Statement – EMG2 Works August 2025 EMG2-BWB-ZZ-XX-RP-CD-0001_SDS (EMG2 Works)

Appendix 8: A42 Culvert Capacity Review



Job No.	Doc No.	Rev.	Page
220500	EMG2-BWB-ZZ-XX-T-W_0009	P02	Page 1
Project		Date Prepared	Prepared by
East Midlands Gatewo	y Phase 2	24/03/25	Robin Green
Title			Authorised by
A42 Culvert Capacity Review		Claire Gardner	

Introduction

The note has been prepared to provide further information in respect to a number of flood risk and drainage related comments raised in the Environment Agency's (EA) scoping opinion of the proposed East Midlands Gateway Phase 2 scheme.

Specifically, the note provides further information relating to the culvert that flows from north to south at the toe of the A42 highway embankment between the EMG2 Works and the Diseworth Brook. In the returned scoping opinion, the EA state: "The Drainage Report should assess if there is sufficient capacity within the piped connection alongside the A42 and consider the risk of blockage and how this would be managed."

This note is based upon the emerging Development Proposals, that are still subject to change.

Existing Arrangements

The EMG2 Works currently falls towards the Hall Brook and the village of Diseworth in the west and the Diseworth Brook in the south. Hyam's Lane, which bisects the site diagonally from the south-west to north-east, is located on the approximate alignment of the catchment break. The generalised topography of the area is illustrated within **Figure 1**.

Ground Investigation completed by Fairhurst has identified that the EMG2 Works is underlain by clayey soils with very poor infiltration rates. During a storm event, when the very limited infiltration capacity of the soils is exceeded, surface water runoff will follow the fall on the topography and flow overland towards the receiving watercourses. To the south of Hyam's Lane a number of field drains/ditches are present that help to intercept and direct overland flows towards the south-eastern corner of the Site. A culvert provides ongoing connectivity beneath Long Holden (a footpath/track located off the southern boundary), and after a very short open reach flows enter a culvert that runs at the toe of the A42 embankment.

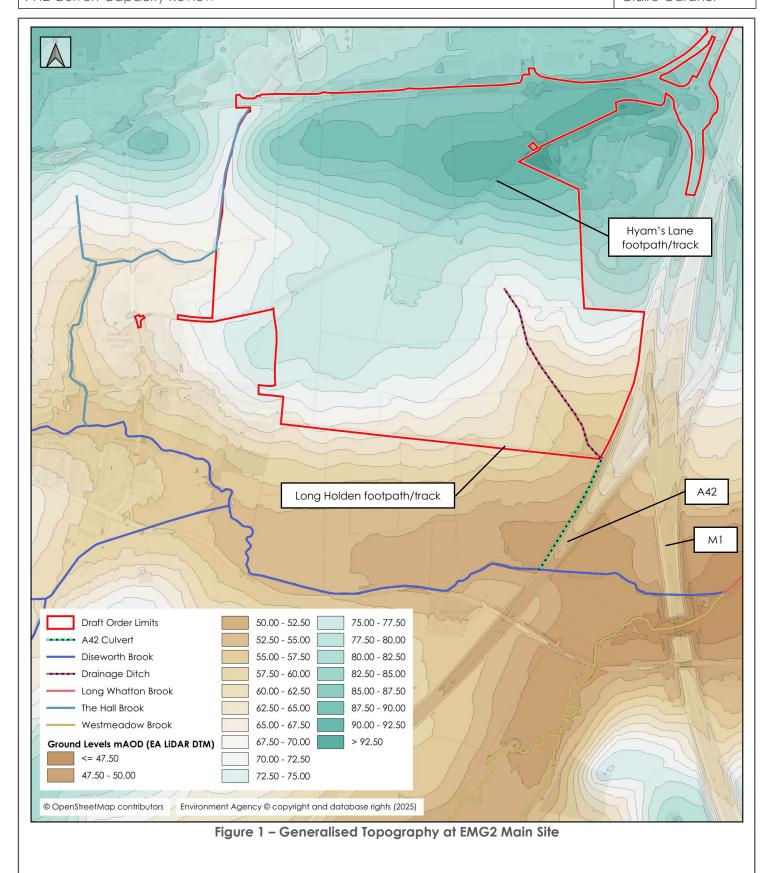
Using the emerging parameters plan for the EMG2 Works, the approximate development area (84ha) and likely impermeable area (69.6ha) have been calculated. Approximately 61% of the developable area is located with the catchment that is currently drained to the A42 culvert – which equates to an impermeable area of 42.4ha. The HR Wallingford UK SUDS greenfield runoff tool was used to estimate the equivalent greenfield runoff rate from the future impermeable area within the current A42 culvert catchment. The rates are summarised within **Table 1**.

Table 1 – Greenfield Runoff Rates

Return Period Storm (yrs)	FEH Runoff Rate (I/s/ha)	Equivalent Runoff Rate from the Total Estimated EMG2 Imp. Area: 69.6ha (1/s)	Equivalent Runoff Rate from the Estimated EMG2 Imp. Area Proposed within the Existing A42 Catchment: 42.4ha (I/s)
1 in 1	2.7	187.9	114.4
Annual Average Runoff Rate (QBAR)	3.3	229.7	139.9
1 in 30	6.6	459.4	279.8
1 in 100	8.4	612.5	373.1
1 in 100+25%	10.5	730.8	445.2
1 in 100+40%	11.8	821.3	500.3



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Job No.	Doc No.	Rev.	Page
220500	EMG2-BWB-ZZ-XX-T-W_0009	P02	Page 2
Project	·	Date Prepared	Prepared by
East Midlands	Gateway Phase 2	24/03/25	Robin Green
Title		·	Authorised by
A42 Culvert C	apacity Review		Claire Gardner





Job No.	Doc No.	Rev.	Page
220500	EMG2-BWB-ZZ-XX-T-W_0009	P02	Page 3
Project		Date Prepared	Prepared by
East Midlands Gatev	vay Phase 2	24/03/25	Robin Green
Title			Authorised by
A42 Culvert Capacity Review			Claire Gardner

A CCTV survey of the downstream A42 culvert connectivity has been completed. The survey has shown that:

- To reach the A42 culvert the runoff from the area first passes beneath the Long Holden footpath/track within a 500dia pipe laid at 1:30 using the Colebrook-White equation a pipe full capacity of 780l/s can be estimated.
- After passing beneath the track, flows enter a 525dia pipe laid at roughly 1:7 this has a pipe full capacity of 1840l/s
- A 700dia pipe then runs at the toe of the A42 embankment eventually outfalling to the Diseworth Brook. This has an average gradient of 1:100 this has a pipe full capacity of 1030l/s.

Proposed Arrangements

The scheme proposes to maintain a connection for the disposal of surface water runoff from the development to the A42 culvert.

In paragraph 59 of the Department for Transport (DfT) Circular 01/2022 and written into the DMRB (CG 501 paragraph 6.3.1) it is stated that where there is already an existing informal or formal connection into the highway drainage system from a proposed development site, the right for a connection may be allowed to continue provided that the flow, rate and quality of the discharge into the highway drainage system remains unaltered or results in a betterment.

Therefore, the discharge rate into the culvert from the development will be restricted to the equivalent 1 in 1-year greenfield rate from the proposed impermeable area that will be located within the current A42 catchment – a rate of 114.4l/s. Additionally, the surface water runoff from the development will receive treatment prior to be discharged. Therefore, the relevant requirements of DfT Circular 01/2022 will be fulfilled.

The proposed peak discharge rate of 114.4/s is well below the downstream pipe capacity and below the existing contributing runoff from the site at larger storms (see **Table 2**). Therefore, it is concluded that there is sufficient capacity within the existing A42 culvert, and that scheme will reduce flows in the culvert in most large storm events.

Table 2 – Greenfield Runoff Rates

Return Period Storm (yrs)	Equivalent Greenfield Runoff Rate from the Estimated EMG2 Imp. Area Proposed within the Existing A42 Catchment (I/s)	Proposed Discharge Rate to the A42 Culvert (I/s)	Percentage Change in Peak Flow to the A42 Culvert
1 in 1	114.4	114.4	0%
Annual Average Runoff Rate (QBAR)	139.9	114.4	-18%
1 in 30	279.8	114.4	-59%
1 in 100	373.1	114.4	-69%
1 in 100+25%	445.2	114.4	-74%
1 in 100+40%	500.3	114.4	-77%

Risk of Blockage

During a site visit it was observed that debris can accumulate at the inlet to the A42 culvert. In the event of blockage, surface water would follow the fall of the topography (see **Figure 1**) and flow southwards at the toe of the A42 highway embankment (over the top of the A42 culvert) before outfalling to the Diseworth Brook just upstream of the culvert outfall.



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Job No.	Doc No.	Rev.	Page
220500	EMG2-BWB-ZZ-XX-T-W_0009	P02	Page 4
Project		Date Prepared	Prepared by
East Midlands (Gateway Phase 2	24/03/25	Robin Green
Title		·	Authorised by
A42 Culvert Co	apacity Review		Claire Gardner

220500	EMG2-BWB-ZZ-XX-T-W_0009	P02	Page 4
Project		Date Prepared	Prepared by
East Midlands Gateway Phase 2 24/03/25		24/03/25	Robin Green
Title			Authorised by
A42 Culvert Capacity Review			Claire Gardner

It is proposed that the inlet to the A42 pipe will be added to the inspection and maintenance regime of the EMG2 Project to ensure that it is kept in good condition to manage the risk of a potential blockage. Furthermore, the runoff from the development will be treated to remove sediments and debris, whereas currently runoff from the agriculture fields can freely enter the pipe system transporting debris and sediment. Therefore, the EMG2 Project is expected to reduce the risk of blockage within the A42 culvert.

East Midlands Gateway 2, Diseworth
Sustainable Drainage Statement – EMG2 Works
August 2025
EMG2:EWB-2Z-XX-RP-CD-0001_SDS (EMG2 Works)

Appendix 9: STW Pre-development Enquiry and Additional Correspondence

WONDERFUL ON TAP



BWB Consulting 11 Portland Street Manchester M1 3HU

25th November 2024

Severn Trent Water Ltd

Leicester Water Centre Gorse Hill Anstey Leicester LE7 7GU

www.stwater.co.uk

Email:

Network.Solutions@SevernTrent.co.uk

Vijay Tanna

Our ref: 1133992

F.A.O: Matthew Bailey

Dear Sir/Madam.

Proposed Development: (Upto 24xIndustrial units -20.83I/s)
North and South of Hyams Lane, Long Whatton and Disewoth, Derby
XY:446000;325000

I refer to your 'Development Enquiry Request' in respect of the above named site. Please find enclosed the sewer records that are included in the fee together with the Supplementary Guidance Notes (SGN) which refer to surface water disposal from development sites.

Protective Strip

Sewer records show a public foul rising main running across your development site. The sewer will require a 10m clearance about the pipe's centreline (5m each side). Please note, no planting of trees or construction should take place within these easements.

Sewer records show a public 300 foul water sewer towards the north west of the site. The sewer will require a 10m clearance about the pipe's centreline (5m each side). Please note, no planting of trees or construction should take place within these easements

Sewer records show a public 375mm surface water sewer towards the south east of the site. The sewer will require a 10m clearance about the pipe's centreline (5m each side). Please note, no planting of trees or construction should take place within these easements.

Due to a change in legislation on 1 October 2011 there may be former private sewers on the site which have transferred to the responsibility of Severn Trent Water Ltd, which are not shown on the statutory sewer records, but are located in your client's land. These sewers would require protective strips of 3 metres either side of the sewer's centreline that we will not allow to be built over. If such sewers are identified to be present on the site, please contact us for further guidance.

WONDERFUL ON TAP



Please note: there is no guarantee that you will be able to build over or close to any Severn Trent sewers, and where a diversion is required there is no guarantee that you will be able to undertake those works on a self-lay basis. Every approach to build near to or divert our assets has to be assessed on its own merit and the decision of what is or isn't permissible is taken based on the risk to the asset and the wider catchment it serves. It is vital therefore that you contact us at the earliest opportunity to discuss the implications of our assets crossing your site. Failure to do so could significantly affect the costs and timescales of your project if it transpires diversionary works need to be carried out by Severn Trent.

Foul Water Drainage

The nearest foul sewers are located in the highway to the west of the site on Grimes Gate and nearest mh is SK4524**3702**. It is anticipated the approximate development of such size would generate approx. foul flows of 20.83l/s (2xdwf).

Due to the nature of the development, the additional flows and existing flood and surcharge levels, there is insufficient capacity within the Severn Trent network and insufficient capacity within the receiving pumping station (Diseworth - Ladygate (SPS)) at present and modelling will be required, which may show that improvements are required to the Severn Trent network.

We are undergoing a prioritisation process of all investment requirements and emerging risks from growth on our network and treatment works as we build our plan for the coming Asset Management Plan period (2025-2030) and beyond.

We will pass the details of your site over for consideration and feedback if anything arises which is of concern. We will let you know as soon as possible if anything will affect your connection points and timescales and whether we need to make representation to the Planning Authority to apply conditions relating to phasing or occupation of the site. This will enable us to understand what system improvements are required due to your proposed development drainage scheme.

In the meantime, the site will be added to our modelling tracker and reviewed regularly until the site can be progressed for sewer modelling. I would therefore be grateful if you would forward as soon as possible the following details:

- Confirmation whether a pumped solution is required (please provide pump rate and frequency, if available), all adoptable pump stations must pump min of 3.8l/s minimal
- Anticipated flow rate from the site
- Proposed planned start and completion date
- Any phasing details of the proposed development

WONDERFUL ON TAP



 Confirm how many properties will discharge into each of the connections to the public sewer.

All connections are subject to the required Section 106 sewer connection application.

Please note for any discharge of non- domestic flows you will need to also consult with our Trade Effluent team via :

trade.effluent@severntrent.co.uk

Surface Water Drainage

Under the terms of Section H of the Building Regulations 2000, the disposal of surface water by means of soakaways should be considered as the primary method. If these are found to be unsuitable, satisfactory evidence will need to be submitted. The evidence should be either percolation test results or by the submission of a statement from the SI consultant (extract or a supplementary letter).

Subject to above Severn Trent Water expects all surface water from the development to be drained in a sustainable way to the nearest watercourse or land drainage channel, subject to the developer discussing all aspects of the developments surface water drainage with the Local Lead Flood Authority (LLFA). Any discharge rate to a watercourse or drainage ditch will be determined by the LLFA / EA.

Note, STW will have to be satisfied that all sustainable option have been exhausted before allowing discharge to the public network. Please note you must ensure to look in to connecting the SW into any nearby watercourses.

Subject to above, a connection to the 375mm surface water sewer and nearest mh SK4624**6501** running across the east of the site can be considered with flows restricted in line with greenfield run off rates of 5l/s per hectare Therefore, a gravity connection to the public sewer (direct or indirect) is acceptable subject to a formal Section 106 sewer connection approval.

Connections

For any new connections (including the re-use of existing connections) to the public sewerage system, the developer will need to submit a Section 106 application form. Our Developer Services department are responsible for handling all new connections enquiries

WONDERFUL ON TAP



and applications. To contact them for an application form and associated guidance notes please call 0800 7076600 or download from www.stwater.co.uk.

Please quote the above reference in any future correspondence (including e-mails) with STW Limited. Please note that Developer Enquiry responses are only valid for 6 months from the date of this letter.

Yours sincerely

Vijay Tanna Network Solutions Developer Services



RE: Development enquiry ref: 1133992- North and South of Hyams Lane, Long Whatton and Disewoth, Derby

From Network Solutions

Date Tue 15/07/2025 12:41

To Matthew Bailey Trade Effluent

Cc Robin Green

This email originated from outside of our organisation. Please exercise caution with content, links and attachments.

ST Classification: OFFICIAL PERSONAL

Good afternoon Matthew

Thank you for your email and thank you for providing the drainage plan and Sustainable Drainage Statement.

Previous modelling was carried out which has highlighted High flooding impact as well as a very high operational impact.

I will get in touch with our growth and planning team to review the site further to confirm the risk level from your proposed connection. Aswell as to understand if any improvement works has since taken place or if anything has been planned in. Or whether we need to make representation to the Planning Authority to apply conditions relating to phasing or occupation of the site.

To expedite the prioritisation process please inform us to as and when you secure the DCO.

Please note from reviewing your drainage plan I understand you are proposing to connect the rising main directly to the to the public foul sewer- however if a connection is permitted any pumped connection would need to be made via a 'break chamber' and short section of gravity sewer, prior to connecting to an existing or new manhole on the public sewer.

For any queries regarding your non domestic flows our Trade Effluent team will be bets to advise further.

Many thanks

Vijay Tanna



Senior Evaluation Technician Network Solutions | Severn Trent Water



WONDERFUL ON TAP



Did you know? You can now make full applications online for a variety of our Developer Service offerings including Development Enquiries. Take a look here for more details: https://www.stwater.co.uk/building-and-developing/regulations-and-forms/application-forms-and-guidance/

We have listened to our customers and local communities and Severn Trent have made a pledge to transform and protect the health of our Rivers, for more information please follow the link below:

https://www.stwater.co.uk/get-river-positive/our-river-pledges/

We always aim for a 10/10 service . If there's anything we can do to make your experience even better , please let us know

From: Matthew Bailey
Sent: 14 July 2025 14:48
To: Network Solutions
Trade Effluent

Cc: Robin Green

Subject: Re: Development enquiry ref: 1133992. North and South of H

Subject: Re: Development enquiry ref: 1133992- North and South of Hyams Lane, Long Whatton and Disewoth, Derby

Caution: This is an external email originating outside Severn Trent. Think before you click on links or open attachments.

Hi Vijay,

Please find attached the latest concept drainage strategy drawing. I have also attached the latest Sustainable Drainage Statement report with the appendices removed (to reduce its file size). Section 5 of this report relates to the foul water drainage strategy.

Let me know if you need any of the other appendices sent across for review.

Please can you confirm receipt of the attached and also a likely timescale for you to review and provide a response?

Thanks,

Matt

Matthew Bailey

Senior Engineer | BWB Consulting Limited



Advance Notice of Annual Leave / Out of Office:

From: Network Solutions
Sent: 08 July 2025 15:29
To: Matthew Bailey Trade Effluent

Cc: Robin Green

Subject: RE: Development enquiry ref: 1133992- North and South of Hyams Lane, Long Whatton and

Disewoth, Derby

This email originated from outside of our organisation. Please exercise caution with content, links and attachments.

ST Classification: OFFICIAL PERSONAL

Good afternoon

Thank you for your email.

Due to cyber security restrictions we are not permitted to access any 3rd party external links/SharePoint folders.

Can you please arrange to share PDF attachments of the proposed drainage plan for this proposed development site for us to review further.

Many thanks





www.stwater.co.uk/building-and-developing





Did you know? You can now make full applications online for a variety of our Developer Service offerings including Development Enquiries. Take a look here for more details: https://www.stwater.co.uk/building-and-developing/regulations-and-forms/application-forms-and-guidance/

We have listened to our customers and local communities and Severn Trent have made a pledge to transform and protect the health of our Rivers, for more information please follow the link below:

https://www.stwater.co.uk/get-river-positive/our-river-pledges/

We always aim for a 10/10 service . If there's anything we can do to make your experience even better , please let us know

From: Matthew Bailey
Sent: 04 July 2025 16:01
To: Network Solutions
Trade Effluent
Cc: Robin Green

Subject: Re: Development enquiry ref: 1133992- North and South of Hyams Lane, Long Whatton and

Disewoth, Derby

Caution: This is an external email originating outside Severn Trent. Think before you click on links or open attachments.

Hi Vijay,

I am emailing to provide an update on this application and hopefully this will allow you to provide further detail to your response and/or prepare for the future connection of this site and undertake any necessary hydraulic modelling works.

I will be emailing separately on the other pre-planning enquiry (reference: 1133855) which is part of the overall scheme. This is an upcoming Development Consent Order (DCO) / Material Consent Order (MCO), so works differently to a typical planning application with limited details on the future occupier uses of the units to be constructed; therefore, if it would be useful to Severn Trent Water Network Solutions Team (I have also looped in the trade effluent team, which I have mentioned below) for us to have a Teams call to discuss the proposals to help coordinate how we prepare for this development then I would be happy to set up a meeting. Please let me know if this would be useful to you.

The 2nd round of statutory consultation started last Friday (27th June) and the drainage strategy is more developed since the initial pre-planning enquiry was submitted.

I have attached the latest proposed project delivery programme. All being well, the construction of the main site will be taking place between Summer 2025 through to Autumn 2023, with enabling works occurring between Summer 2026 through to Summer 2028, with building occupations starting from January 2027 with completion by September 2030.

The latest drainage strategy, and accompanying conceptual drainage strategy drawing, can be downloaded from this link - 250407 EMG2 DCO - Drainage Strategy

We are proposing for foul flows to drain within the site to one (or multiple if necessary) terminal pumping station(s) which will then discharge foul flows to the public foul sewer network. There are two potential separate foul public sewers locate within the A453 at the north site boundary which we hope to utilise.

Given the nature of a DCO application, the final configuration of the development will not be confirmed until the DCO application has been approved; however, based on the latest parameters plan (which the DCO would be approved based on), there would be a maximum allowable development floorspace of **30ha** across the site. We have the opportunity to utilise foul water attenuation within the site to allow us to limit the maximum discharge rate from any pumping stations to facilitate a connection(s) into the foul public sewer network.

You have asked for additional details in your pre-planning response which I have copied and replied to below in **blue**.

- Confirmation whether a pumped solution is required (please provide pump rate and frequency, if available), all adoptable pump stations must pump min of 3.8l/s minimal
- This is to be confirmed (TBC) and will only be known once the development is being built out; however, we can utilise foul water attenuation within the site to control our maximum foul discharge rate to work with STW as necessary to facilitate the connection of the development to the public sewerage system.
- Anticipated flow rate from the site

Again, TBC; however, you have suggested that will be approximately 20.83I/s based on the old parameters plan for the site (latest parameters plan has been attached). We can work with STW to set this rate if required.

- Proposed planned start and completion date
- See attached delivery programme.
- Any phasing details of the proposed development
- See attached delivery programme.
- Confirm how many properties will discharge into each of the connections to the public sewer.

 Anywhere between 7-24 total units to be constructed, with a maximum total floorspace delivered

across the site of 30ha. The attached delivery programme suggest that 11 units will be constructed at this stage.

I trust the above and attached allows you to undertake your modelling works and/or advise on the viability of the future connection(s) of this upcoming development. Please do let me know if you need any additional information or would like a meeting to discuss the proposals and options for how the site is delivered to facilitate a connection to the public sewerage network without resulting in any adverse impacts to the wider network, whilst also not delaying the delivery programme of the development.

Trade Effluent

At this stage, we do not know who the occupier of the unit will be and therefore we do not know if any trade effluent will be generated. Therefore, I'd also be keen to get the trade effluents thoughts on who we as a collect prepare for the upcoming DCO application, as it's likely that the future occupier of the unit won't be determined until the DCO application has been approved and the unit is being built out. Therefore, we might need to prepare for a potential future occupier that has wet trade effluent to provide resilience to the drainage proposals.

If you could please review the above and attached and confirm back to me if there is anything else you need from us to help STW prepare for this site coming forwards, please can you advise.

Thanks,

Matt

Matthew Bailey

Senior Engineer | BWB Consulting Limited



Advance Notice of Annual Leave / Out of Office:

07/07/25 - 12/07/25

From: Network Solutions

Sent: 25 November 2024 15:31

To: Matthew Bailey

Subject: Development enquiry ref: 1133992- North and South of Hyams Lane, Long Whatton and Disewoth,

Derby

This email originated from outside of our organisation. Please exercise caution with content, links and attachments.

ST Classification: OFFICIAL PERSONAL

Good afternoon

Please find attached below our Developer Enquiry response letter, along with a sewer record extract and supplementary guidance notes with regard to the above site.

If you have any further queries with regard to our response, please do not hesitate to contact us on the number / email address mentioned below. Please refrain from sending responses to a certain individual directly. Our email address below will ensure that your response is logged and tracked for a response. When responding, please quote our reference number above in all return correspondence.

(reply to

Kind regards,

Vijay Tanna



Senior Evaluation Technician Network Solutions Severn Trent Water





